

Power Conversion Systems enabled by SiC-based Monolithic Bidirectional FET (BiDFET)

Subhashish Bhattacharya

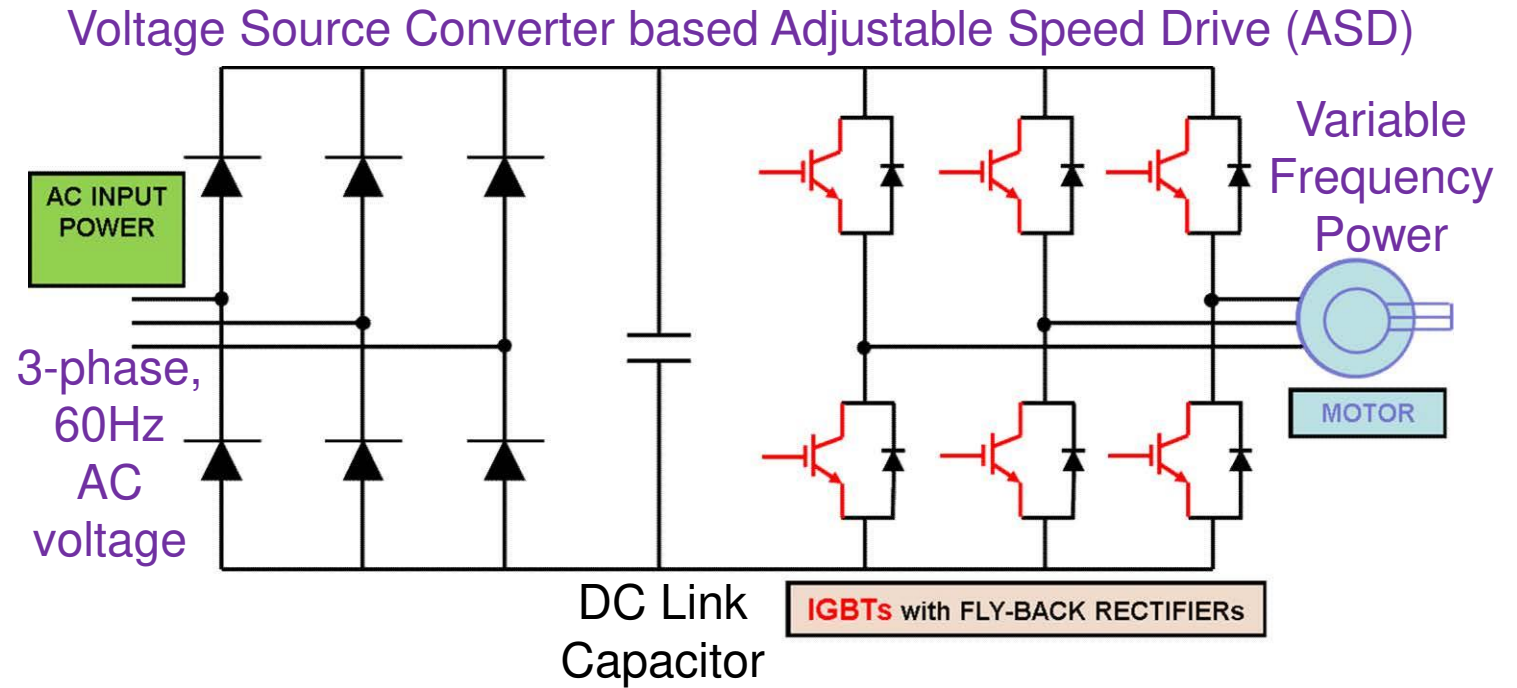
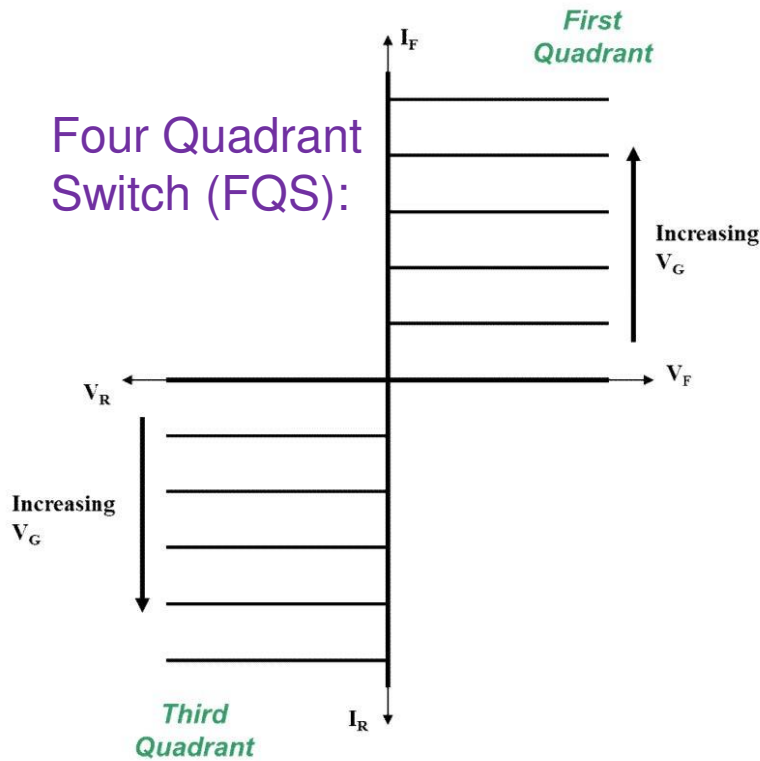
Prof. Jay Baliga – SiC BiDFET device

Prof. Doug Hopkins – Advanced packaging of SiC BiDFET device

FREEDM Annual Meeting 2024 Presentation

April 2, 2024

Four Quadrant Switch (FQS): The Ideal Power Device (The Holy Grail)



Ideal Device Characteristics:

- Large Forward & Reverse Blocking Capability
- Bi-directional current flow
- Zero On-State Voltage Drop
- Fast Switching Capability
- Gate Voltage Controlled Output Characteristics
- Excellent Safe-Operating-Area

ASD needs Energy Storage Element:

- DC link capacitor as energy storage element
- Bulky
- Expensive
- Poor Reliability
- Degraded performance under high temperature
- Single point failure

B. J. Baliga, Fundamentals of Power Semiconductor Devices, 2nd Edition, Springer-Science, 2019

B. J. Baliga, "The IGBT Device", Elsevier, 2015

Four Quadrant Switch (FQS) Enabled Direct AC-AC Matrix or Cyclo Converter

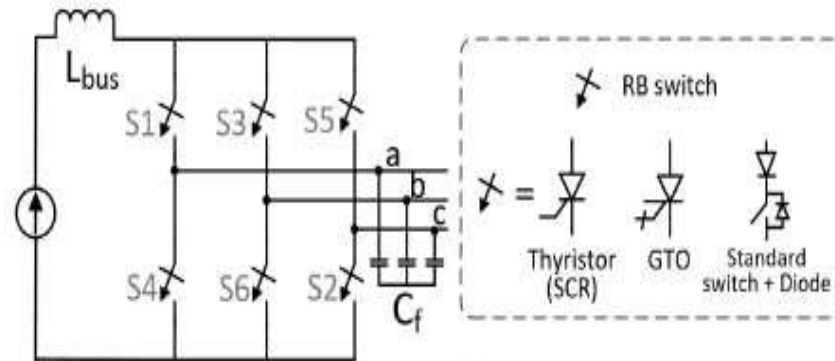
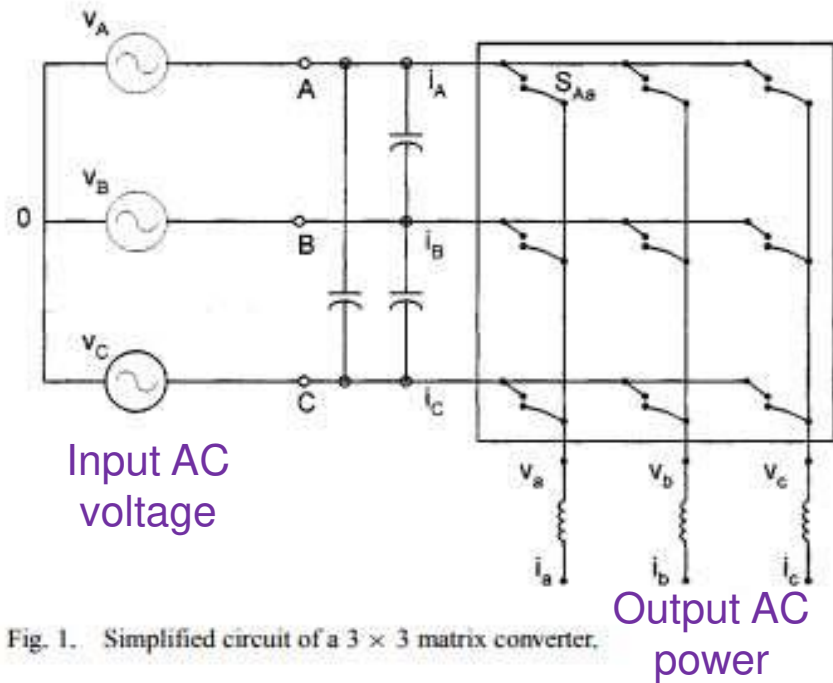
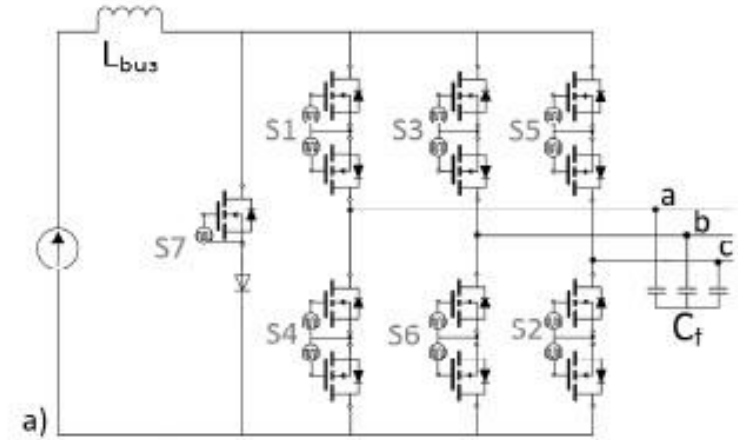


Fig. 1: Conventional CSI topology (H6-CSI) using reverse-voltage-blocking (RB) switches with regulated front-end dc-link current



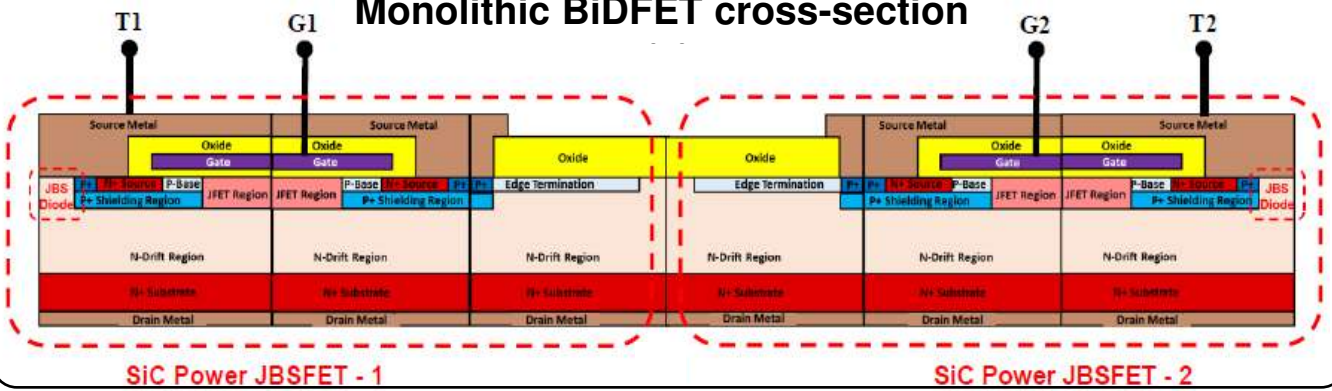
CSI with Bi-Directional [RB] Switches

Fig. 1. Simplified circuit of a 3×3 matrix converter.

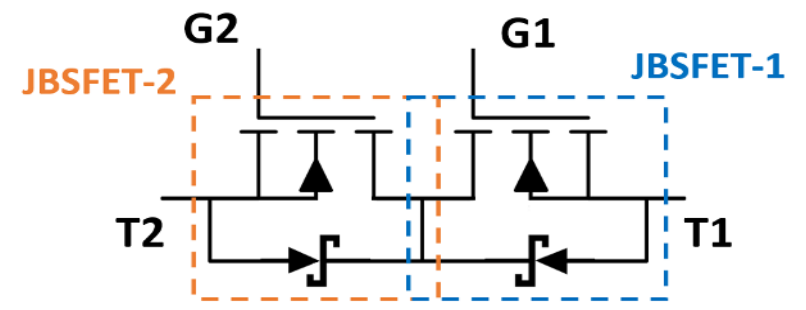
- Direct AC-AC Matrix or Cyclo Converter creates a variable output voltage with unrestricted frequency using an array of fully controlled four-quadrant bidirectional switches
- Does not need large energy storage element and DC-Link
- “Unfortunately, there were no such devices available” and “Consequently, multiple discrete devices had to be used to construct suitable switch cell” [P.W. Wheeler, et al, “Matrix Converters: A Technology Review”, IEEE Trans. Industrial Electronics, vol. 49, no. 2, pp. 276–288, April 2002.]
- CSI have traditionally used Thyristor family reverse voltage blocking (RB) switches [eg. Thyristors, SGTO Thyristors, Symmetric IGCTs] – however, Thyristor family RB switches typically have low switching frequency
- WBG based SiC MOSFET with series connected SiC JBS [Junction Barrier Schottky] diode provides a RB switch with increased switching frequency for CSI – however, will have higher conduction voltage drop compared to single MOSFETs or IGBTs
- SiC BiDFET as a monolithic devices offers advantage of lower conduction voltage drop and higher switching frequency for CSI and Direct AC-AC Matrix or Cyclo Converter based power conversion systems

Monolithic SiC-based Bidirectional FET (BiDFET) Switch: 1200V, 20A DIE

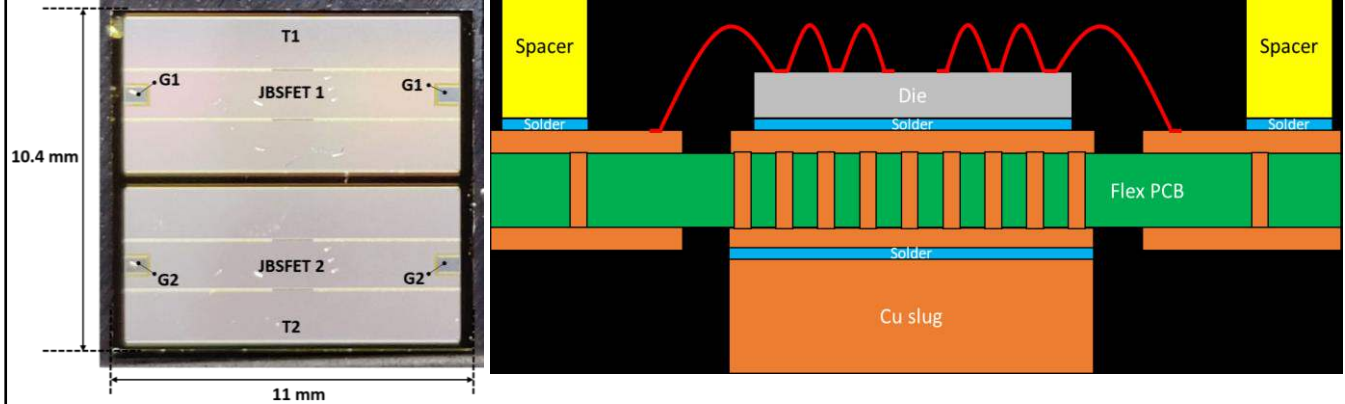
Monolithic BiDFET cross-section



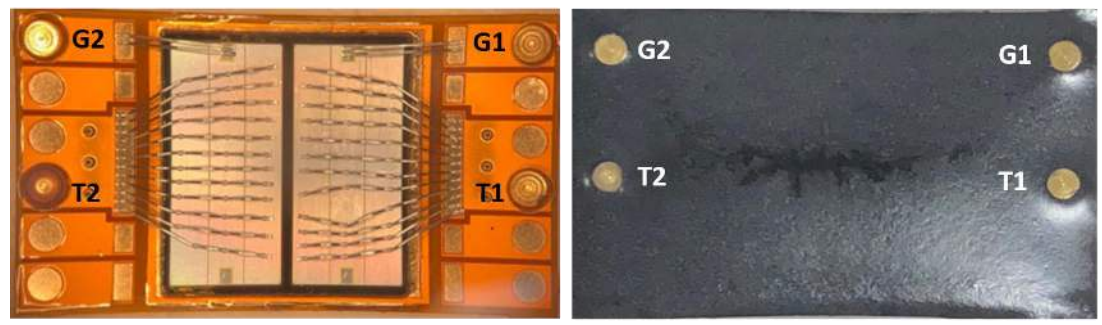
4-terminal Monolithic BiDFET circuit schematic



Fabricated BiDFET die:



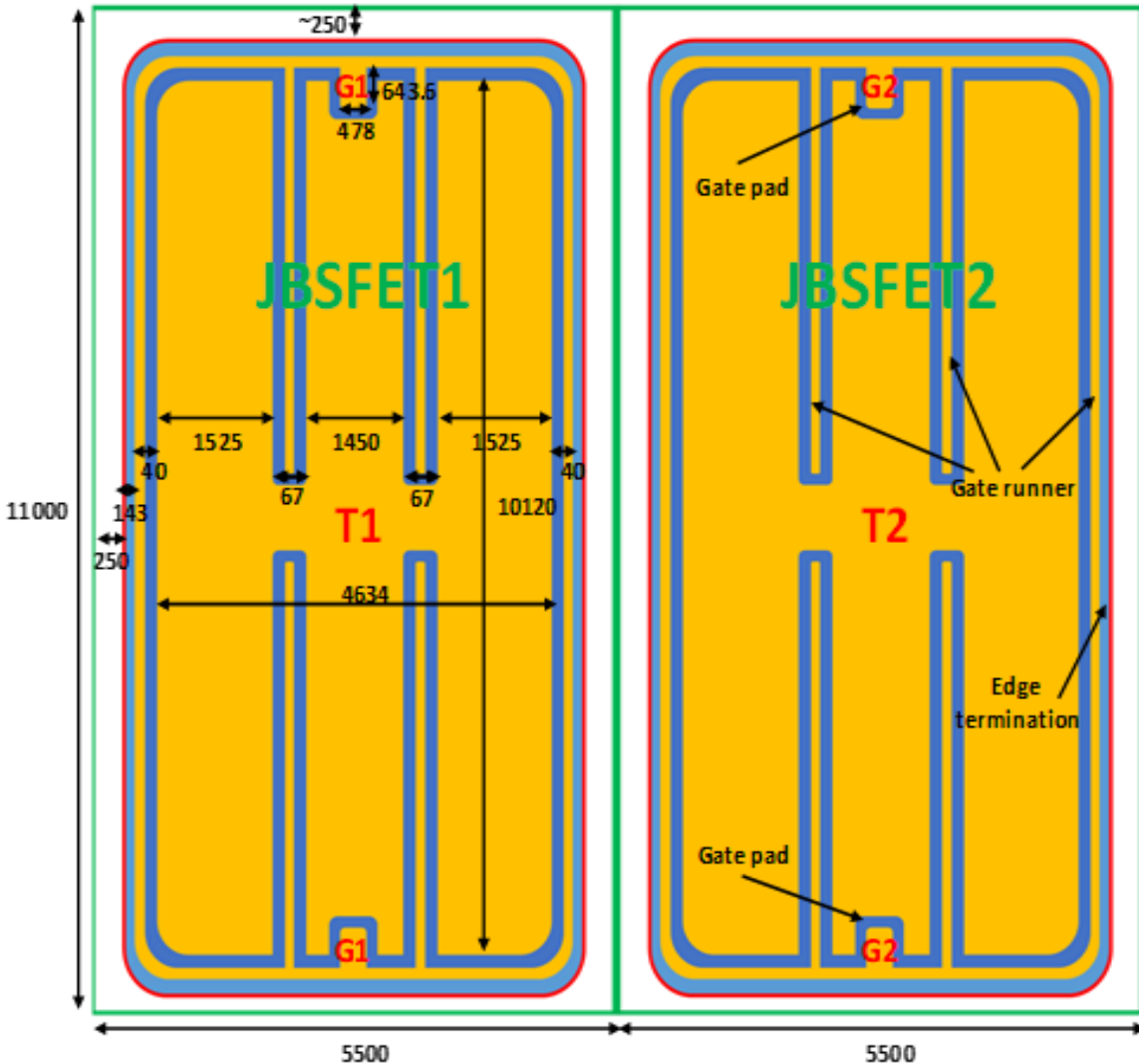
Custom-made 4-terminal package for the BiDFET:



Comparison of fabricated 1.2 kV 20 A BiDFET with previous bidirectional switch implementations

Switch Configuration	Description	Number of components	On-State Voltage Drop (V)	Switching Loss
	Diode Bridge + Asymmetric IGBT <small>Neft & Schauder, IEEE Trans. Ind. Appl., vol. 28, pp. 546-551, 1992</small>	5	8.6 [2 diodes + 1 IGBT]	High
	Asymmetric IGBTs + Freewheeling diodes <small>Moghe et al., ECCE, pp. 3848-3855, 2012</small>	4	5.8 [1 diode + 1 IGBT]	High
	Back-to-back symmetric IGBTs <small>Takei et al., ISPSD, pp. 413-416, 2001</small>	2	2.2 [1 symmetric IGBT]	Very High
	SiC Power MOSFETs + JBS diodes <small>Safari et al., IEEE Trans. Power Electron., vol. 29, no. 5, pp. 2584-2596, 2014</small>	4	3.1 [1 diode + 1 MOSFET]	Low
	Back-to-back SiC Power MOSFETs + antiparallel and series JBS diodes <small>Ahmed et al., IEEE Trans. Power Electron., vol. 32, pp. 1232-1244, 2017</small>	6	3.1 [1 diode + 1 MOSFET]	Low
	Four-terminal SiC Monolithic BiDFET	1	1.0 [1 BiDFET]	Low

Gen-1 SiC BiDFET: Chip Design



Objective 1:

- Rated Blocking Voltage = 1.2 kV
- Breakdown Voltage > 1.4 kV
- Use Hybrid JTE Edge Termination BV > 1.6 kV

Objective 2:

- On-Resistance of BiDFET = 50 mΩ
- Each JBSFET On-Resistance = 25 mΩ
- Use JBSFET Active Area = 0.45 cm²

Objective 3:

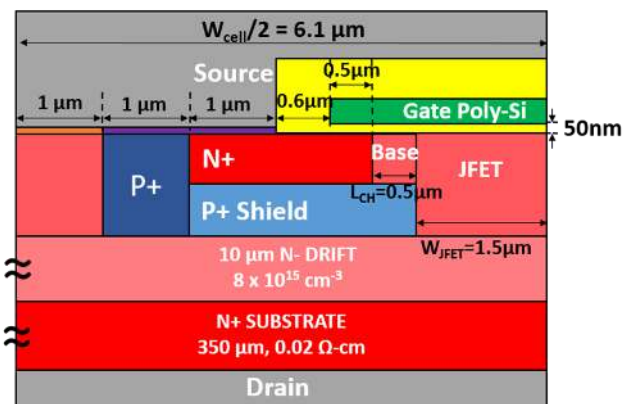
- Low Internal Gate Resistance < 1 Ω
- Use Gate Runners

Objective 4:

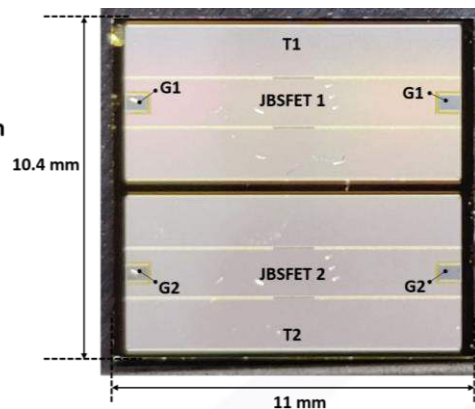
- Improved Packaging and Board Interconnect
- Use Two Gate Bonding Pads per JBSFET

SiC BiDFET Gen-1: Single Chip

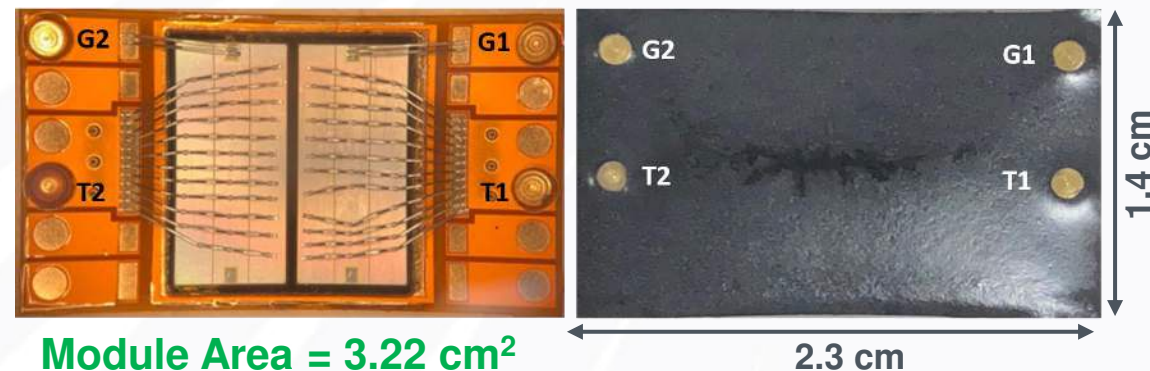
Internal JBSFET cross-section



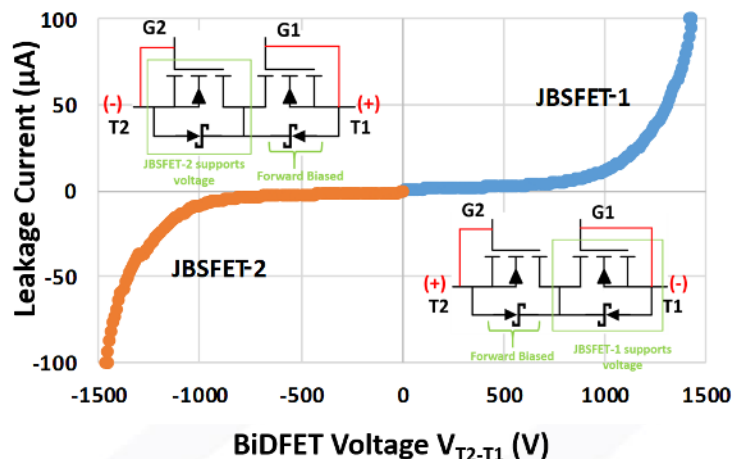
Fabricated BiDFET die



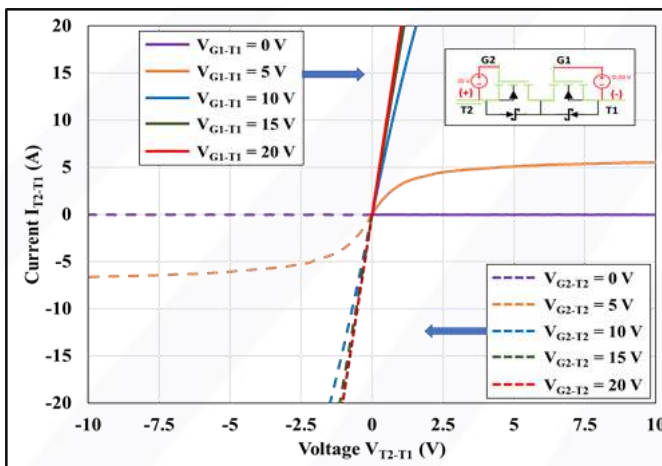
Custom-designed 4-terminal package for the BiDFET



BiDFET blocking characteristics



BiDFET output characteristics

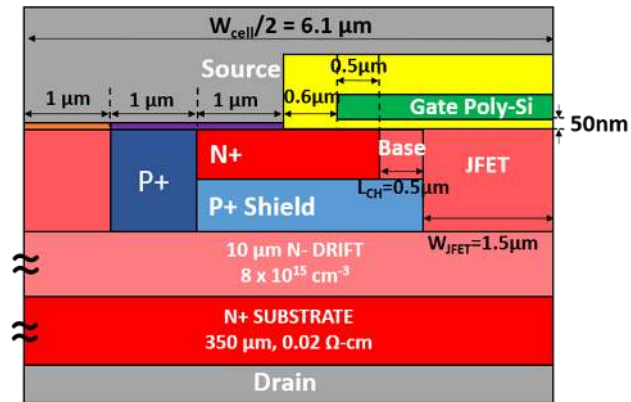


- Blocking Voltage > 1400 V
- On-Resistance = 50 mΩ
- First Pass Success
- Used to demonstrate 1φ 2.3 kW converter
- $C_{iss} = 11,000 \text{ pF}$
- $C_{oss} = 500 \text{ pF}$ at 1000 V
- $C_{rss} = 50 \text{ pF}$ at 1000 V

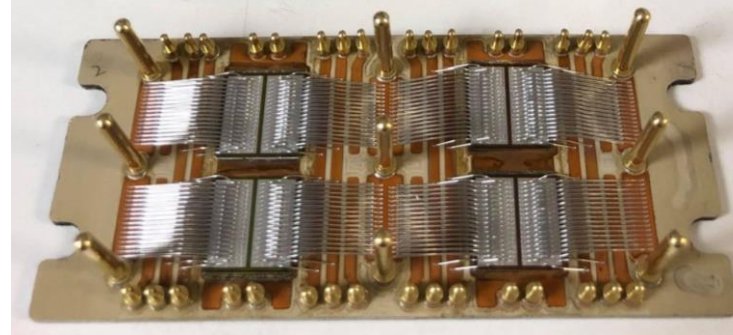
SiC BiDFET Gen-1: Parallel Chips

Objective: Demonstrate Reduced On-Resistance BiDFET by Paralleling Two Chips for 3 ϕ Converter Application

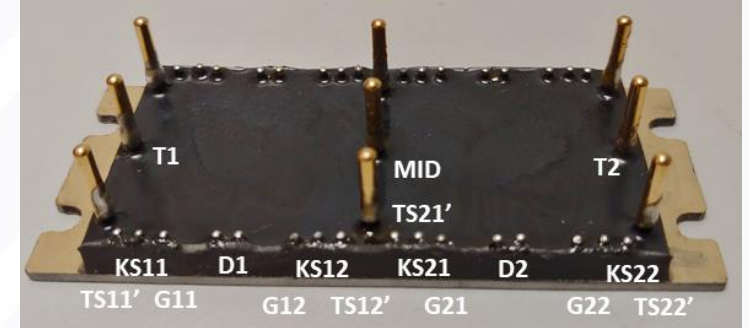
Internal JBSFET cross-section



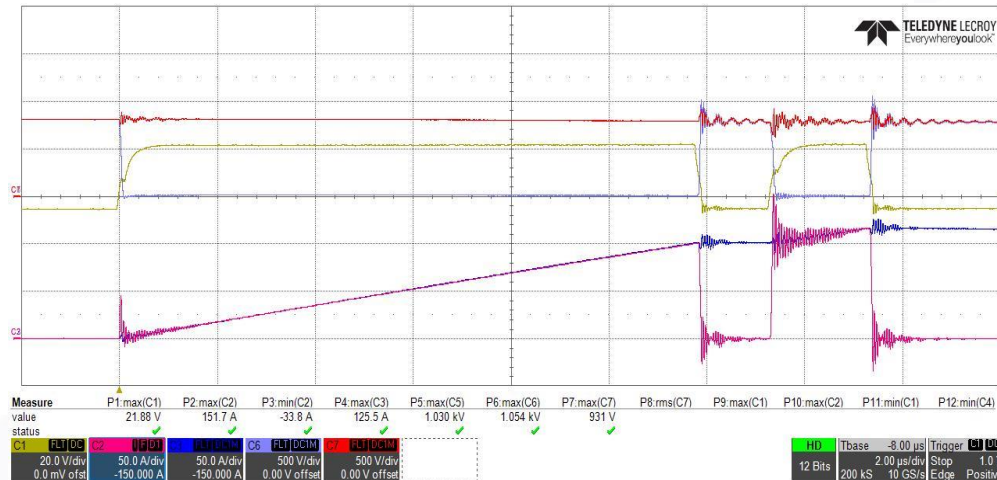
Custom-designed Half-Bridge Module with Paralleled BiDFET chips



Module Area = 27 cm²

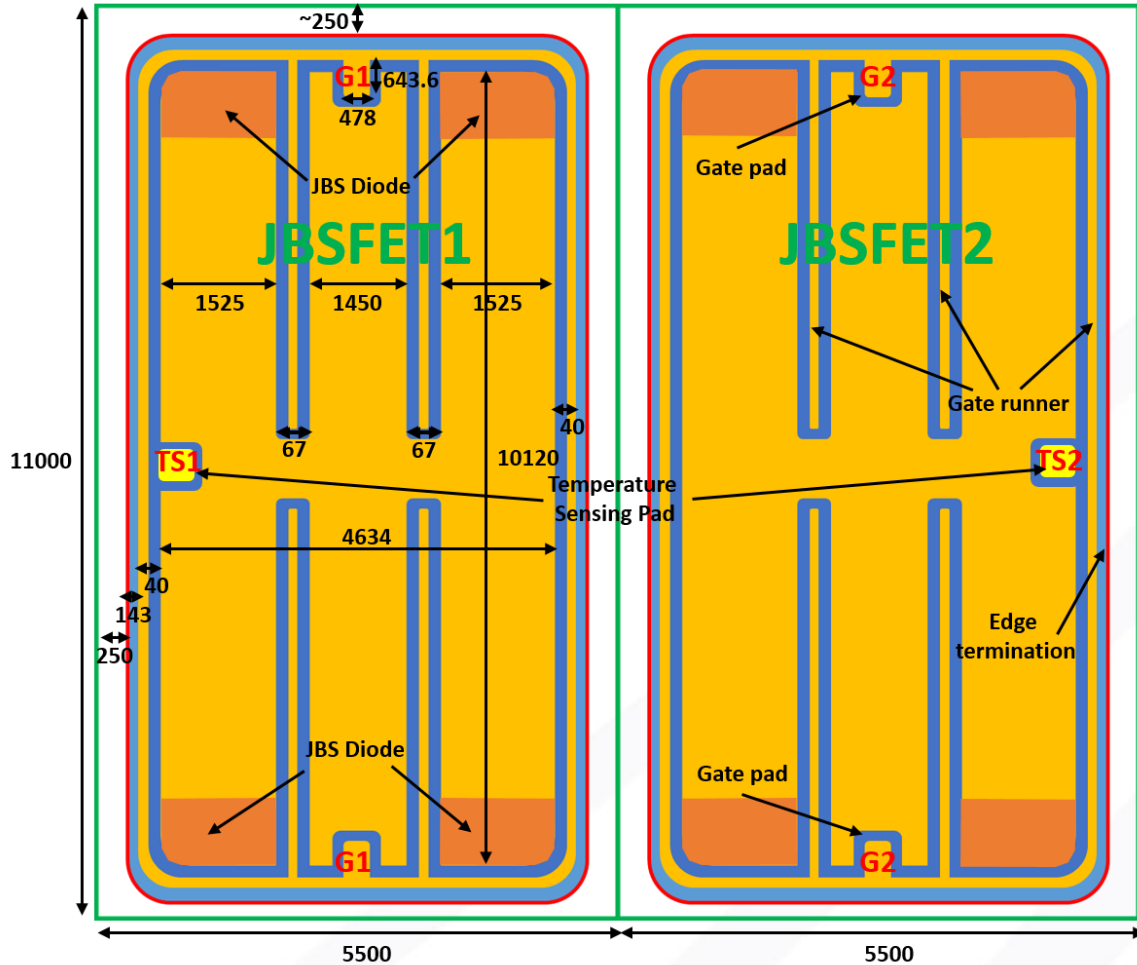


BiDFET DPT Switching Waveforms



- Turn-on and Turn-off like a single Gen-1 BiDFET chip
- Switching Losses (800 V, 20 A):
 - $E_{ON} = 1350 \mu\text{J}$
 - $E_{OFF} = 460 \mu\text{J}$
 - $E_{TOTAL} = 1810 \mu\text{J}$

Gen-2 BiDFET: Achieve 2x Lower R_{on}



Objective:

- Rated Blocking Voltage = 1.2 kV
- Breakdown Voltage > 1.4 kV
- Device On-Resistance = 25 mΩ

Conventional Doubling Die Size Approach:

- Very Low Yield
- Die Size exceeds X-Fab Maximum Reticle Size
- Impossible

Parallel Gen-1 Dies:

- Achieved in Modules

New Design and Process Strategy Created:

- Separate JBS Diode from MOSFET Cells
- Reduces Cell Pitch to 2.8 μm from 6.1 μm
- Reduces Specific On-Resistance to 5.3 mΩ-cm²
- Ascribe 10 % Active Area to JBS Diode
- R_{on} = 26 mΩ achievable

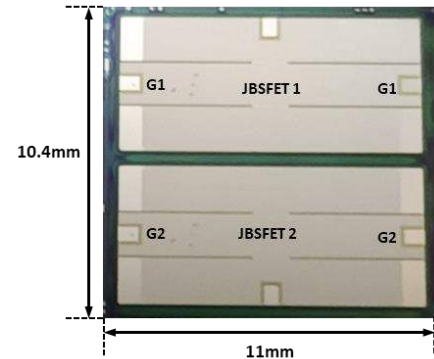
Additional Objective:

- Add Integrated Temperature Sensor
- Use Poly-Silicon Gate Electrode Resistance
- No additional processing required

SiC BiDFET Gen-2 Single Chip

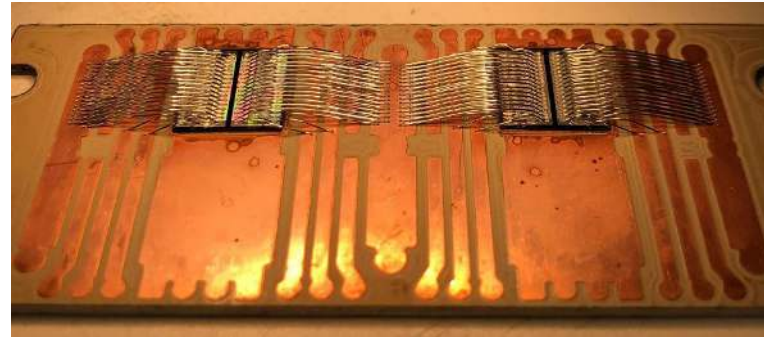
Objective: Demonstrate Reduced On-Resistance BiDFET with Single Chip for 3 ϕ Converter Application

Gen 2 BiDFET Chip

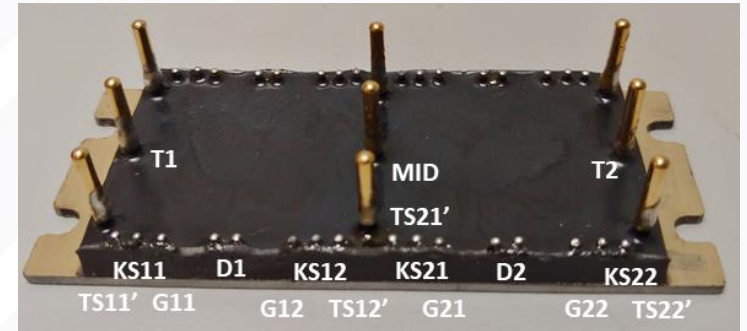


Die Size: 10.4 mm x 11 mm

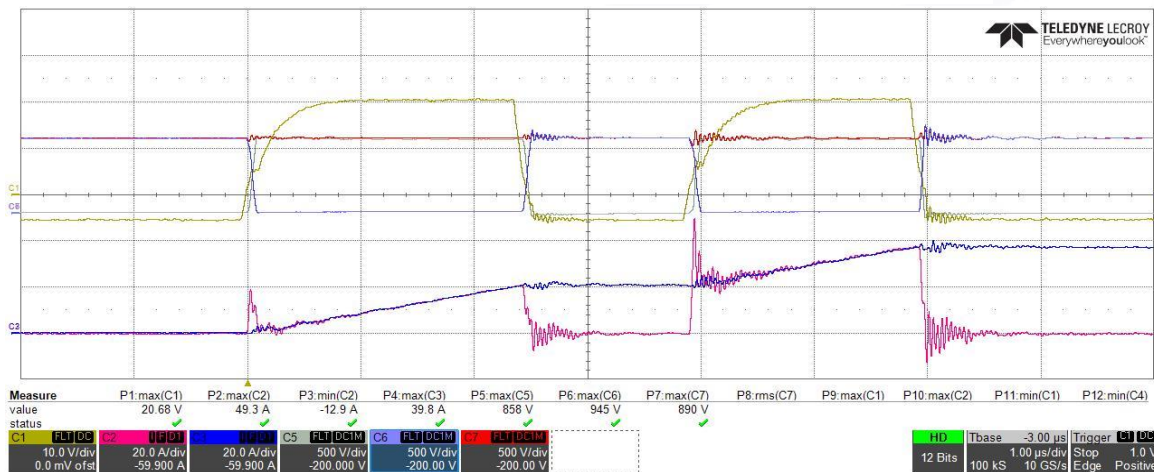
Custom-designed Half-Bridge Module with Single Gen-2 BiDFET Chip



Module Area = 13.5 cm²



BiDFET DPT Switching Waveforms



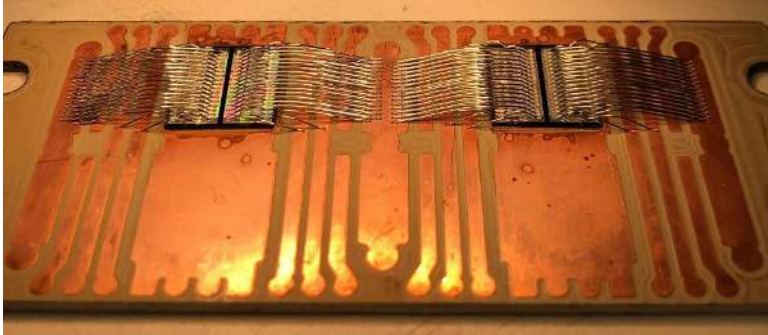
- Turn-on and Turn-off like a single Gen-1 BiDFET chip
- Switching Losses (800 V, 20 A):
 - $E_{ON} = 1120 \mu\text{J}$
 - $E_{OFF} = 250 \mu\text{J}$
 - $E_{TOTAL} = 1370 \mu\text{J}$

Single Gen-2 BiDFET chip can handle 20 A ($V_{ON} = 0.5$ V).

SiC BiDFET Single Gen-2 Chip vs BP-1 Two Gen-1 Chips in Parallel

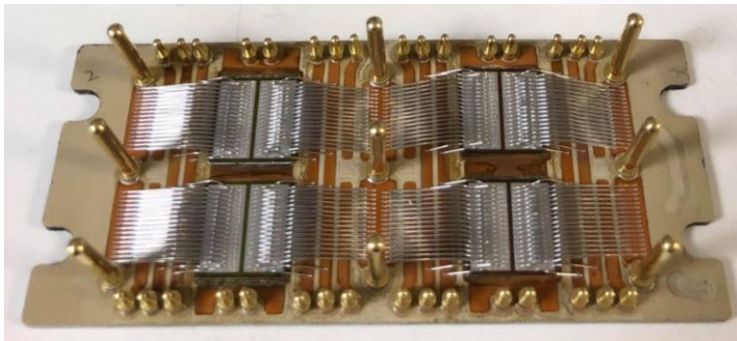
Objective: Demonstrate Reduced On-Resistance BiDFET with Single Chip for 3 ϕ Converter Application

Module with Single Gen-2 BiDFETs



Area = 13.7 cm²

Module with Two Gen-1 BiDFETs in Parallel

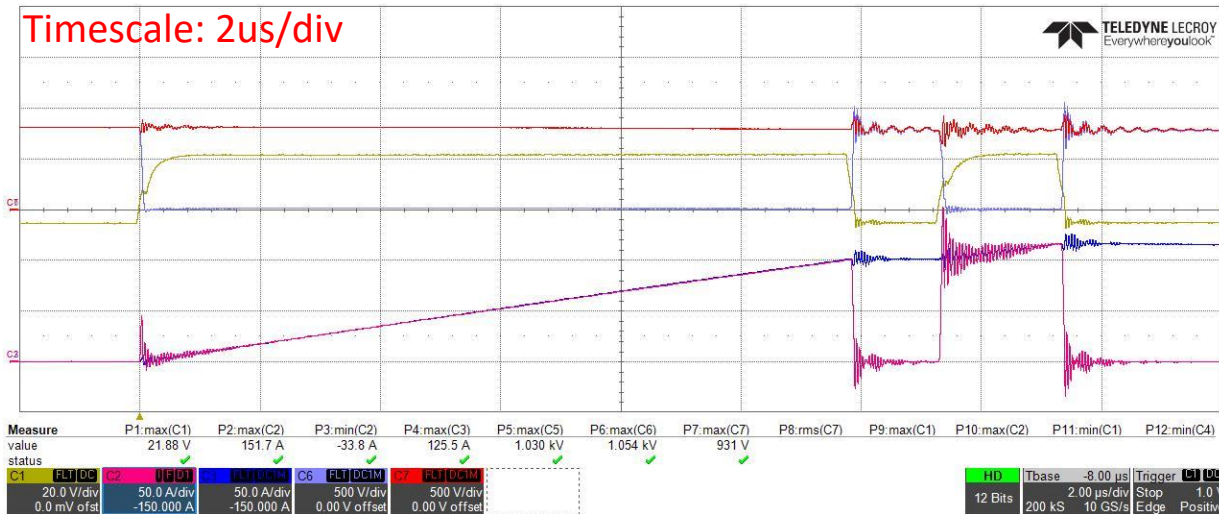


Area = 27.4 cm²

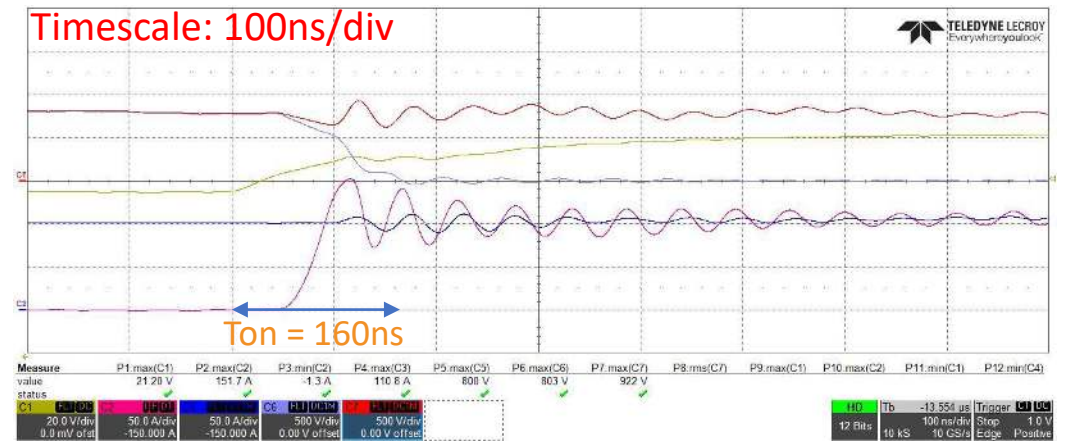
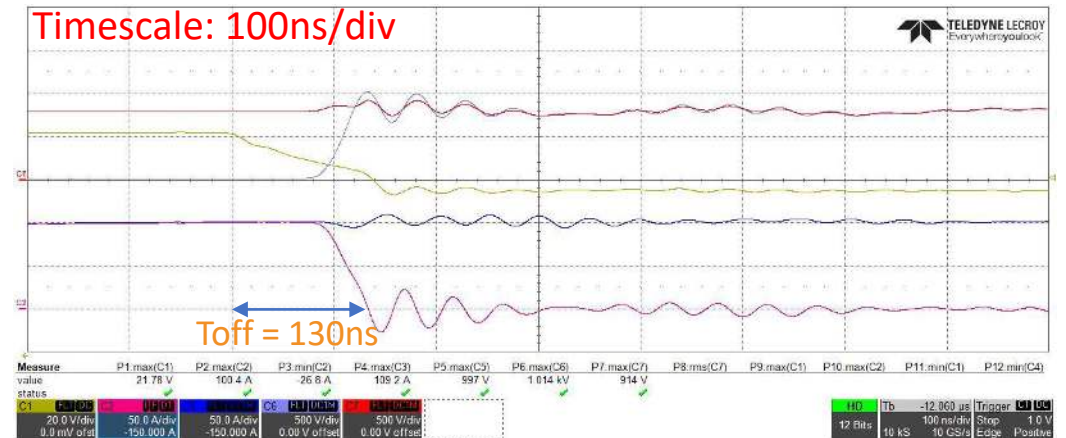
Parameter, Units	Gen 1 (2 Chips)	Gen 2 (1 Chip)	Improvement
Chip Area, cm ²	2.28	1.14	2x
R _{DS,ON} , m Ω	25	27	-
g _M , S	15	15	-
C _{ISS} , pF	15100	11730	1.3x
C _{OSS} , pF	1050	600	1.75x
C _{RSS} , pF	70	70	-
E _{ON} , μ J	1350	1120	1.2x
E _{OFF} , μ J	460	250	1.8x
E _{TOTAL} , μ J	1810	1370	1.3x

BiDFET characterization

DPT results of BiDFET module with two Gen-1 dies in parallel at 800V, 100A.

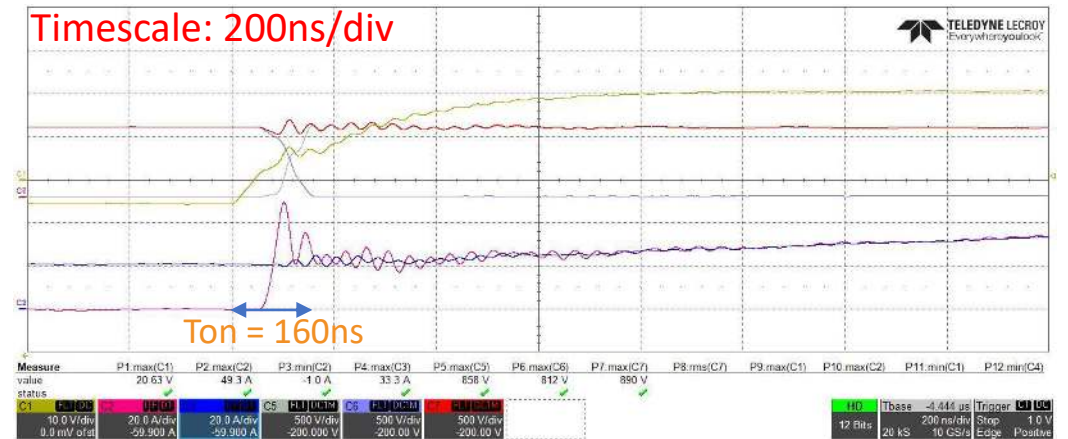
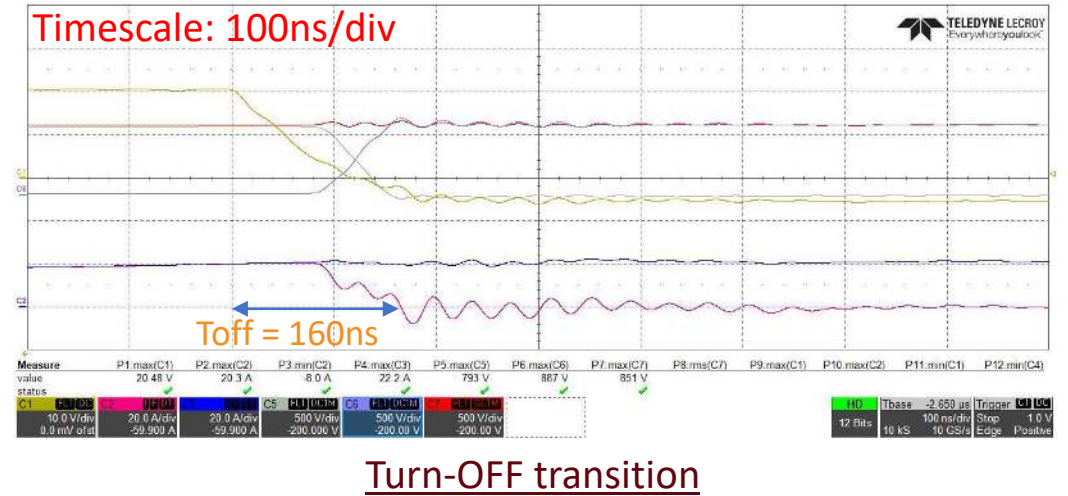
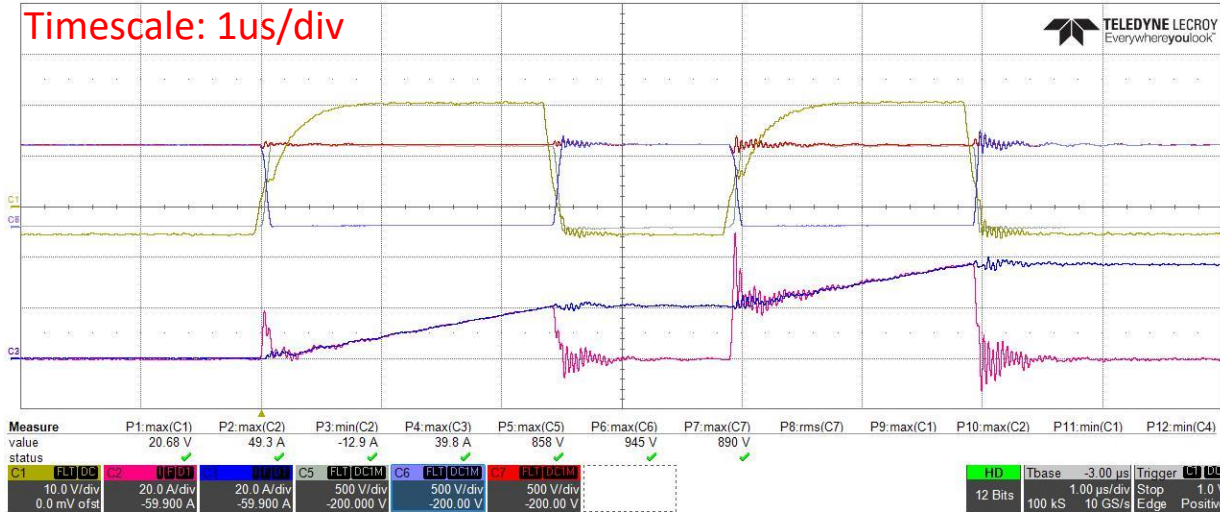


- Channel 1: Gate-source voltage (20 V/div)
- Channel 2: DUT current (50 A/div)
- Channel 3: Inductor current (50 A/div)
- Channel 6: DUT voltage (500 V/div)
- Channel 7: DC bus voltage (500 V/div)



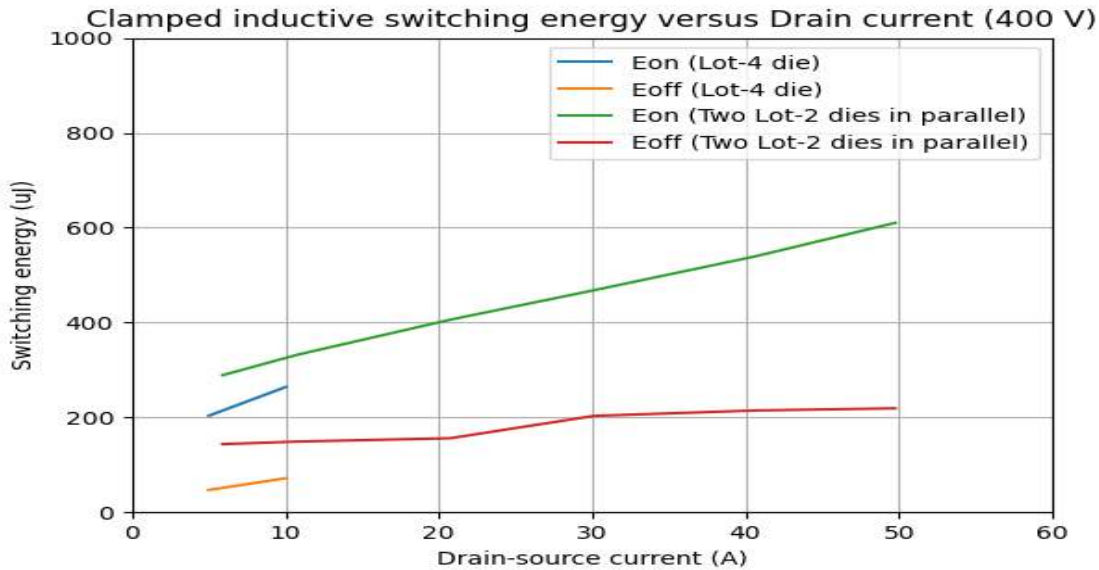
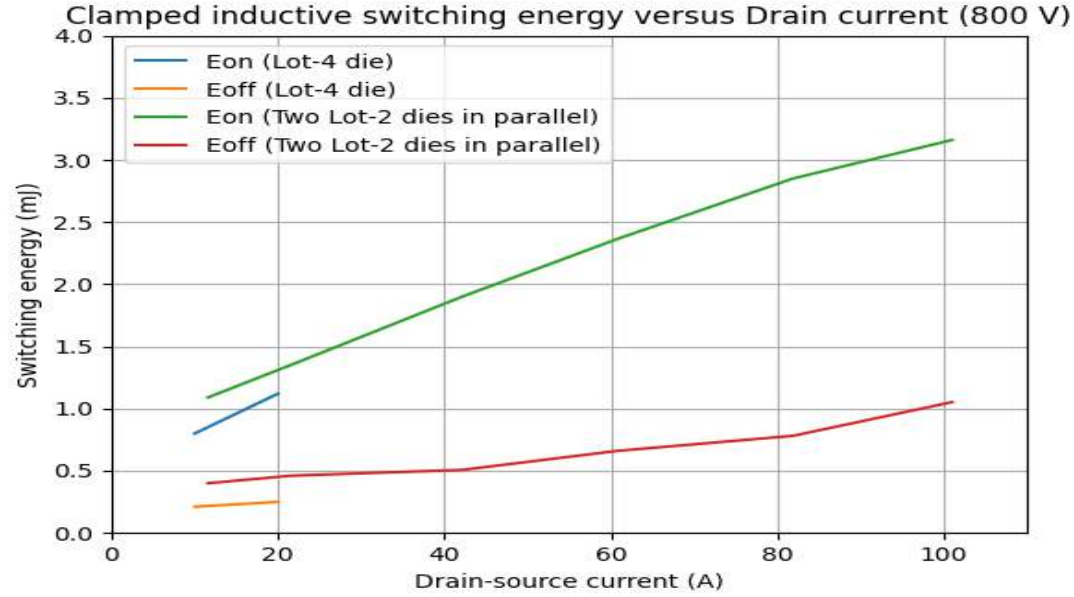
BiDFET characterization

DPT results of BiDFET module with Gen-2 dies at 800V, 20A.



- Channel 1: Gate-source voltage (10 V/div)
- Channel 2: DUT current (20 A/div)
- Channel 3: Inductor current (20 A/div)
- Channel 5: Freewheeling device voltage (500 V/div)
- Channel 6: DUT voltage (500 V/div)
- Channel 7: DC bus voltage (500 V/div)

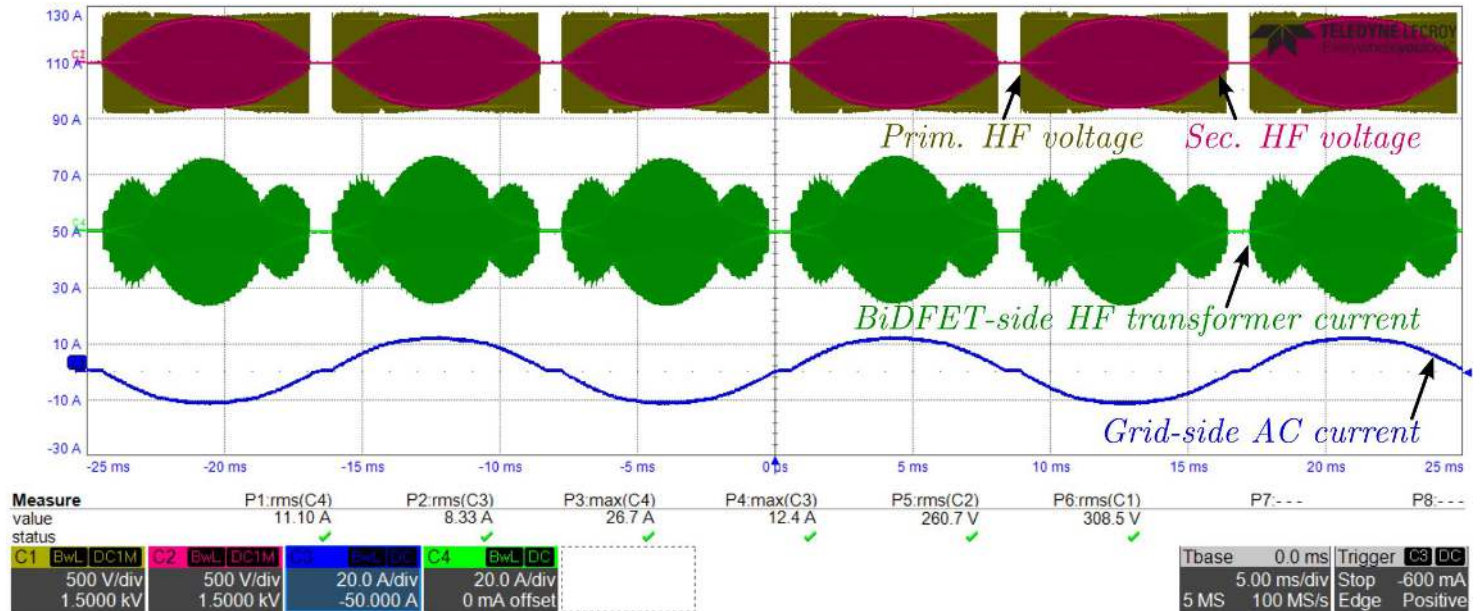
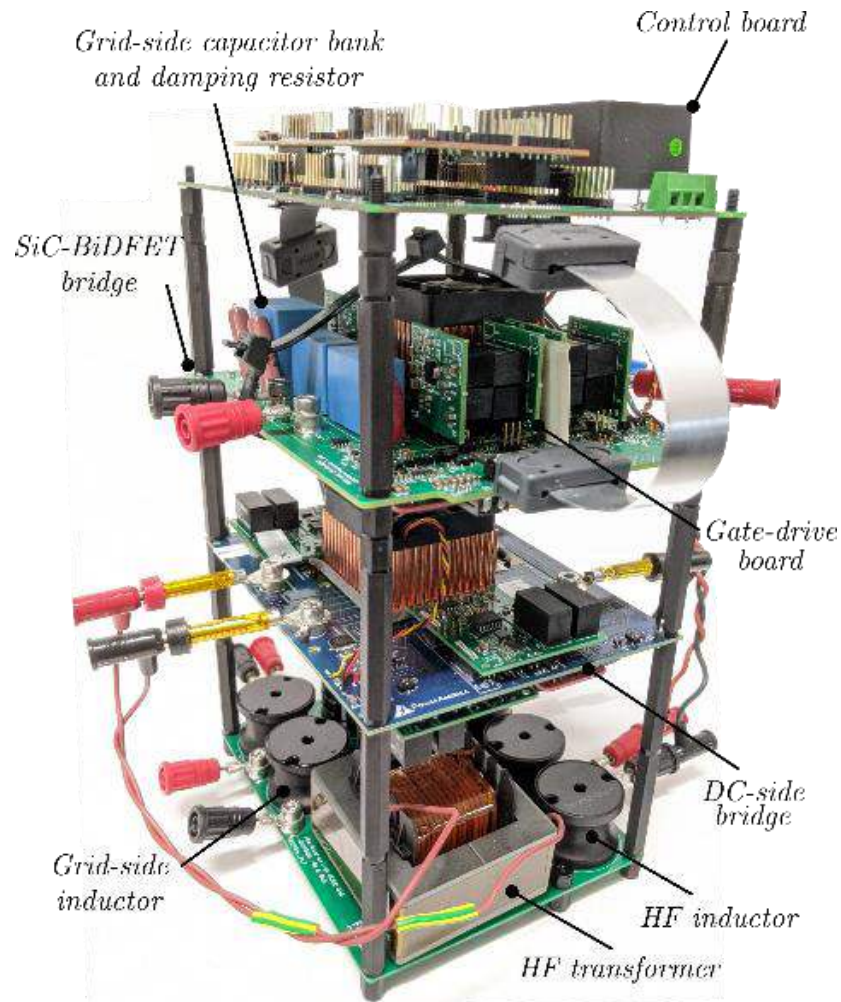
BiDFET characterization



BiDFET	Vds (V)	Ids (A)	Eon (mJ)	Eoff (uJ)	Esw (mJ)
Two Gen-1 dies in parallel ($R_{g, on} = 3.3\Omega$, $R_{g, off} = 1\Omega$)	800	11.6	1.09	399.78	1.49
		21.5	1.35	460.58	1.81
		42.1	1.90	507.20	2.41
		60.8	2.36	660.30	3.02
		81.9	2.85	781.20	3.63
	400	101.0	3.16	1051.50	4.21
		5.9	0.29	143.58	0.43
		10.8	0.33	149.00	0.48
		20.7	0.41	156.05	0.57
		30.1	0.47	203.14	0.67
Gen-2 die ($R_{g, on} = 7.5\Omega$, $R_{g, off} = 2\Omega$)	800	40.7	0.54	214.60	0.75
		49.7	0.61	219.05	0.83
	400	10.0	0.80	211.00	1.01
		20.0	1.12	249.67	1.37
		5.0	0.20	47.00	0.25
		10.0	0.26	71.71	0.33

Dynamic characterization of BiDFET modules at 400V and 800V operation.

2.3 kW, 1-ph grid connected converter prototype enabled by 1200V, 20A SiC BiDFET



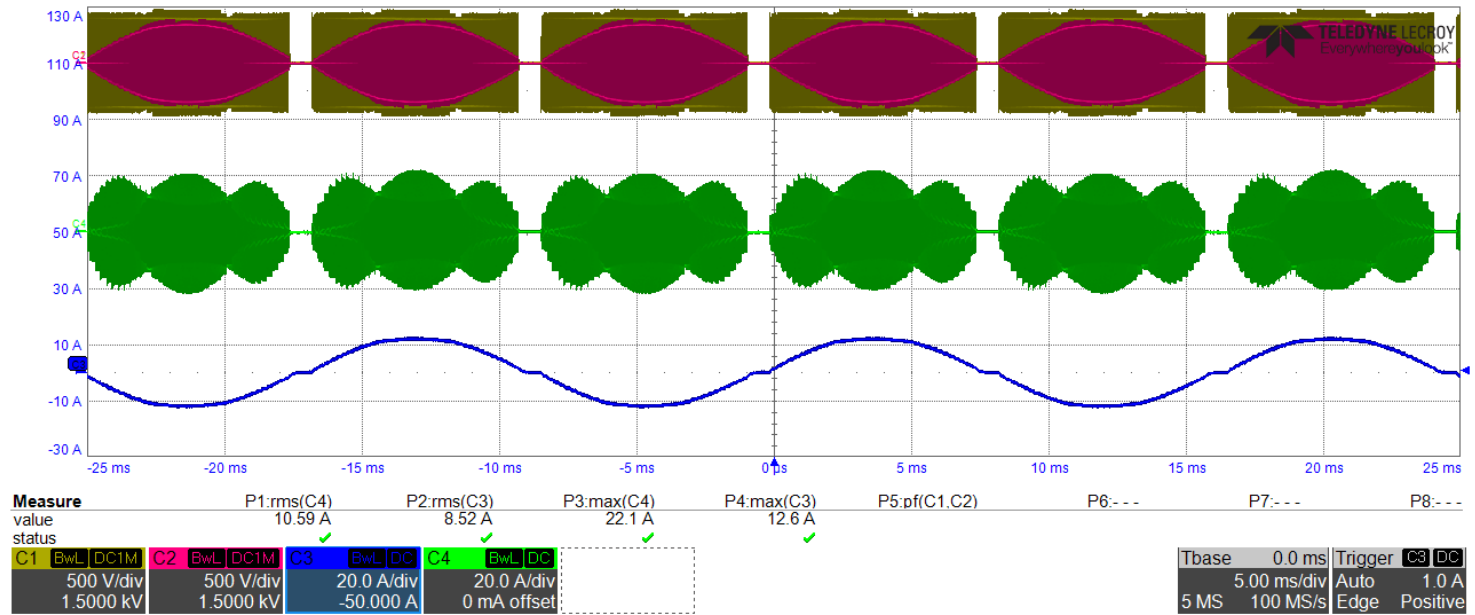
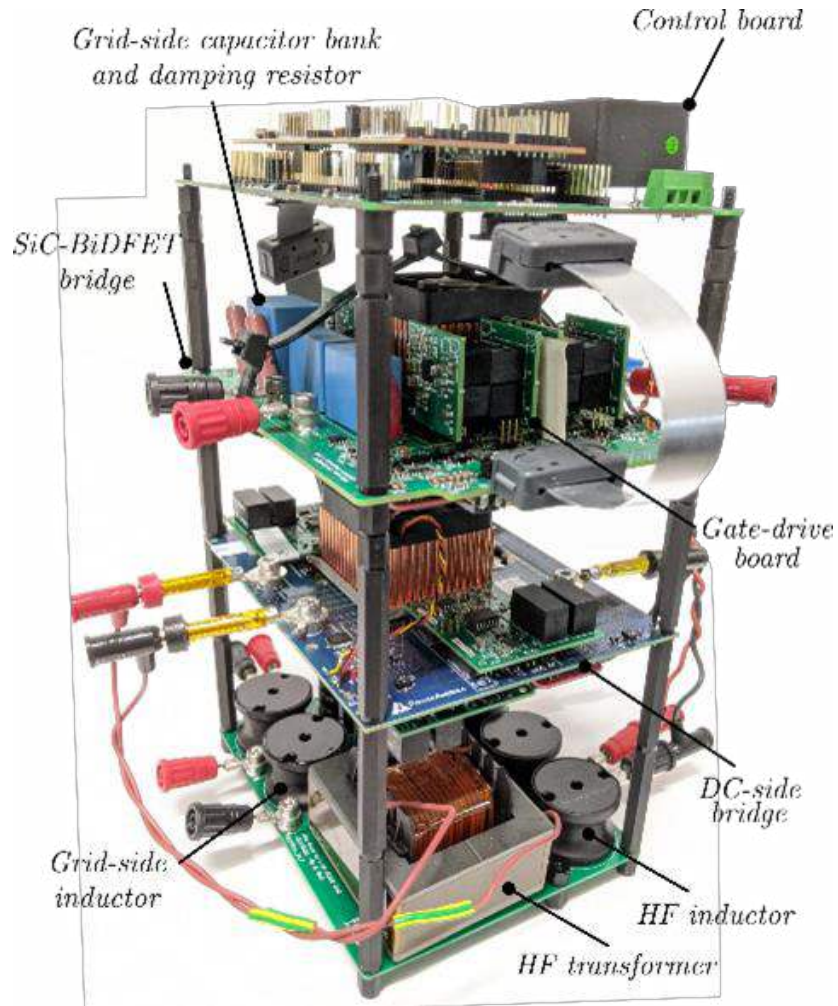
High frequency transformer voltages/current and grid side current at 100% load at 277 V AC voltage.

- Full load operation at 400 V input, 277 V RMS AC output at 2.3 kW power.
- Total harmonic distortion in grid-side current: 4.7%
- Power factor: 0.9998

Hardware prototype of the AC/DC DAB converter for

400 V DC input and 120V/240V/277V AC output.

2.1 kW, 1-ph grid connected converter prototype enabled by 1200V, 20A SiC BiDFET

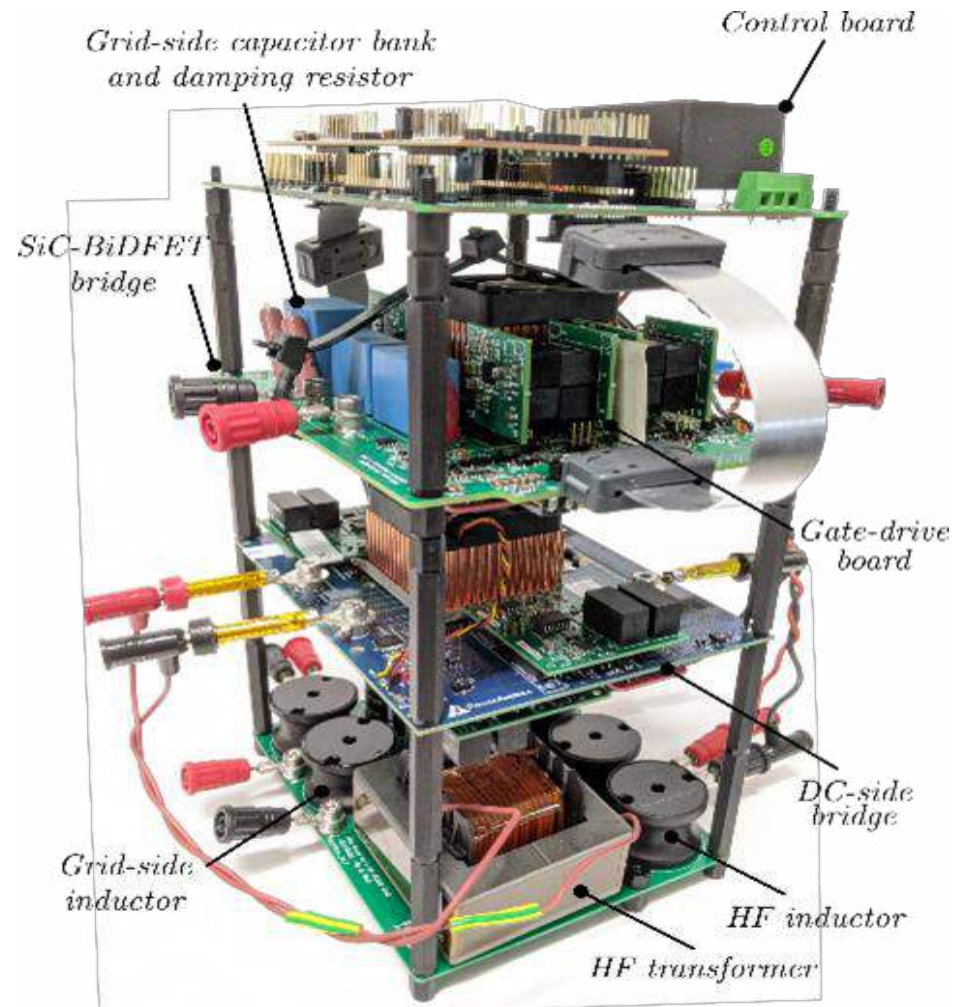


High frequency transformer voltages/current and grid side current at 100% load at 240 V AC voltage.

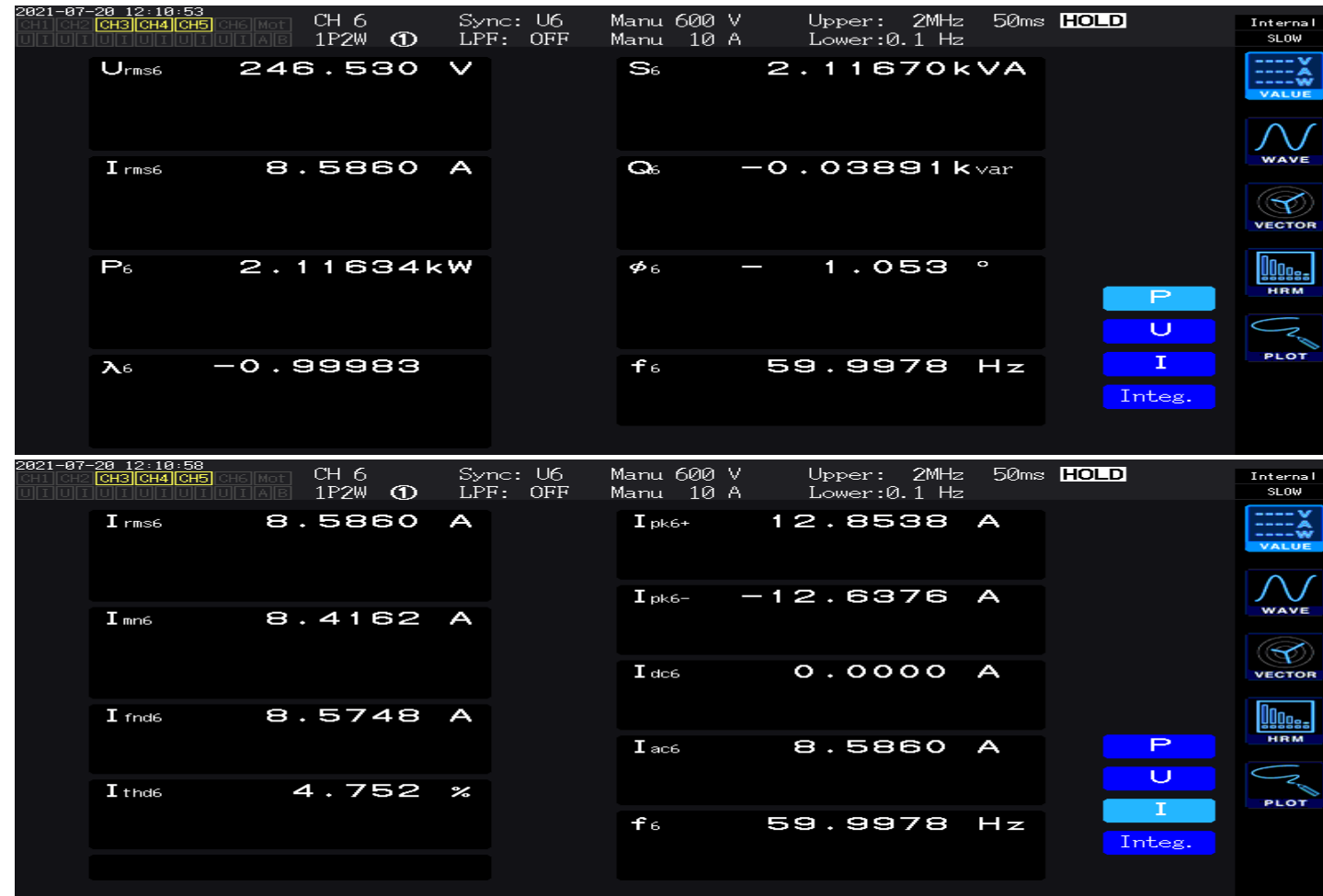
- Full load operation at 400V input, 240V RMS output at 2.1 kW
- Total harmonic distortion in grid-side current: 4.8%
- Power factor: 0.9998

Hardware prototype of the AC/DC DAB converter

2.1 kW, 1-ph grid connected converter prototype enabled by 1200V, 20A SiC BiDFET



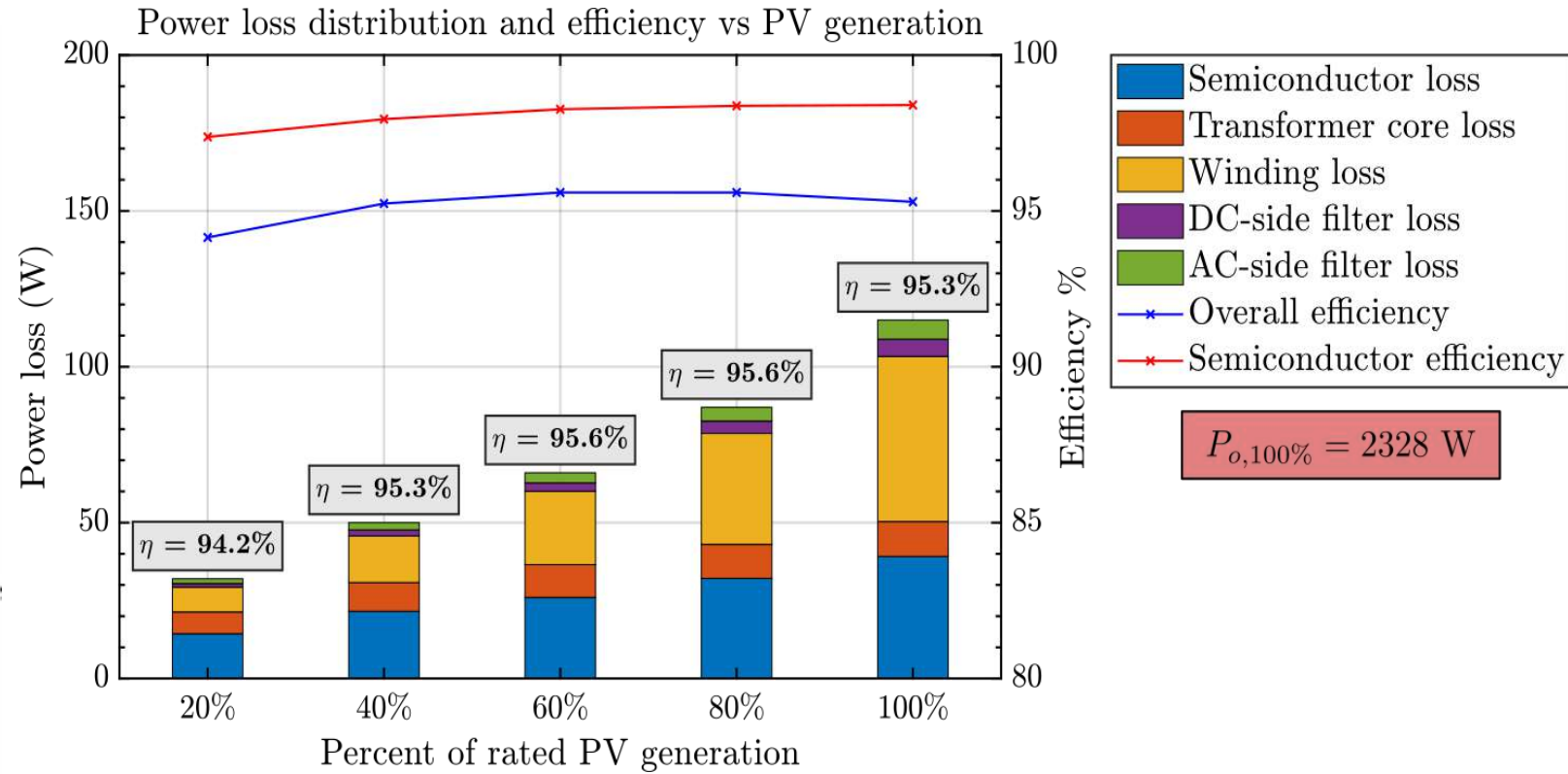
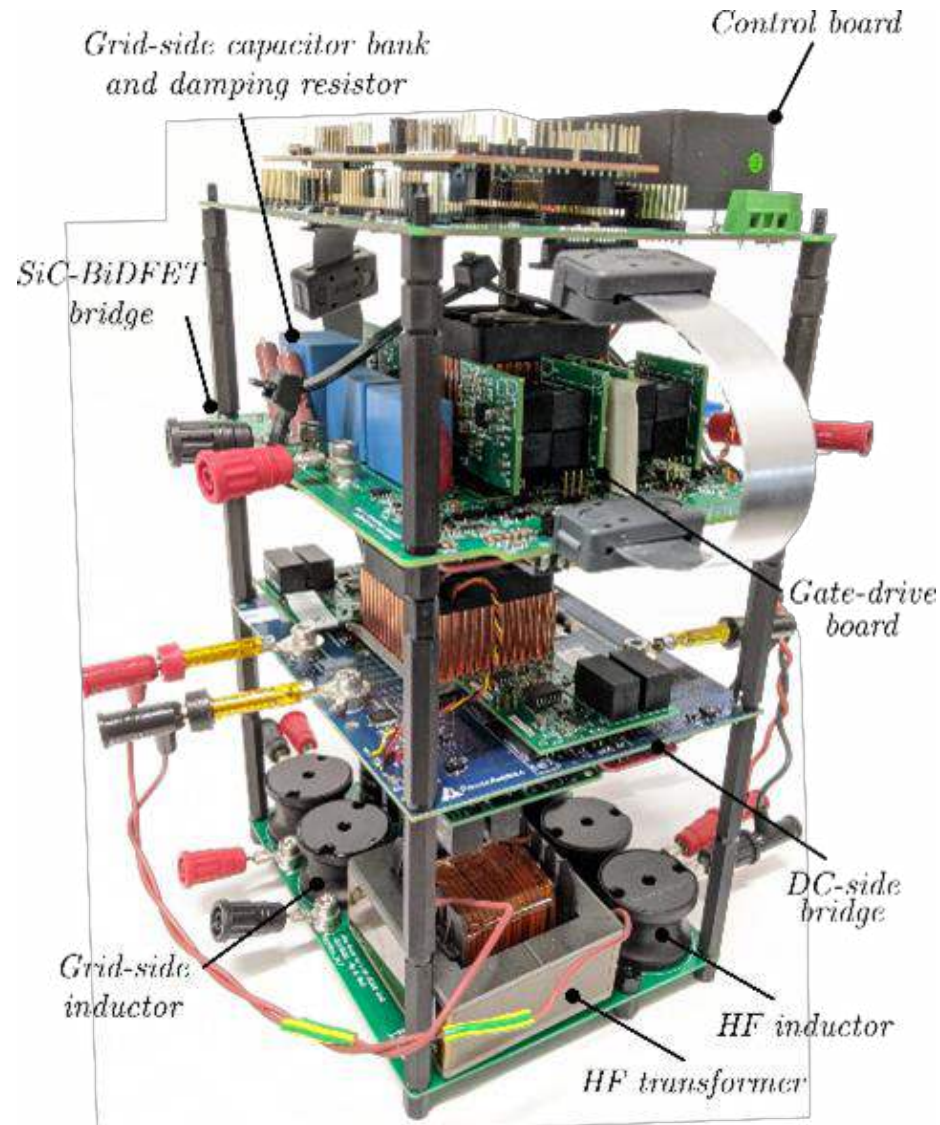
Hardware prototype of the AC/DC DAB converter



Power factor and current total harmonic distortion at 100% load at 240 V AC voltage.

- Measurement using Hioki Power Analyzer PW6001.
- Current sensors: 50 A, 2 MHz.
- Voltage potentiometers: 1000 V.

2.1 kW, 1-ph grid connected converter prototype enabled by 1200V, 20A SiC BiDFET

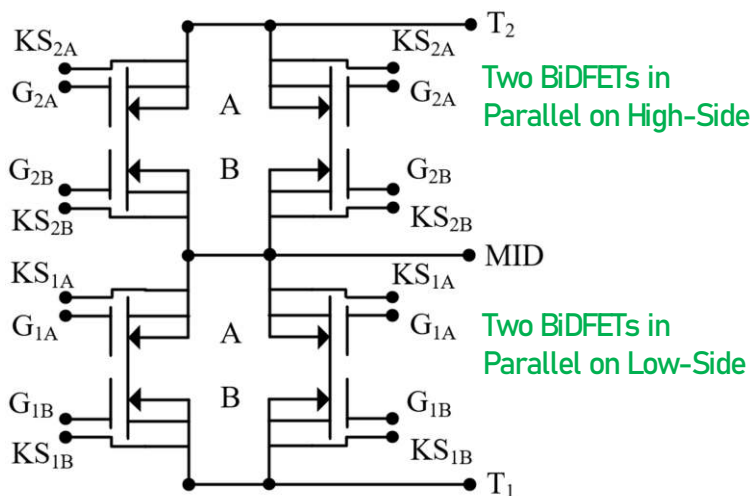


Overall efficiency, semiconductor efficiency and estimated loss distribution at different rates of PV generation.

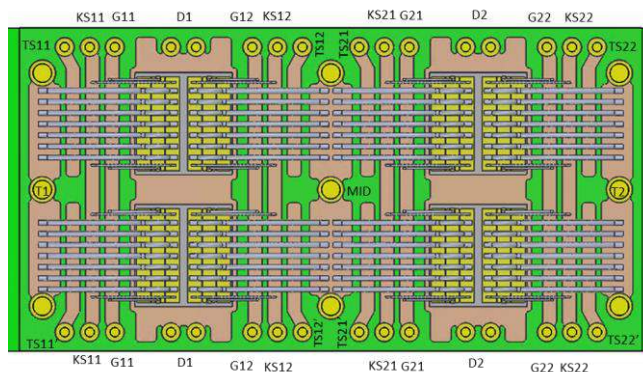
- Semiconductor efficiency indicates losses in the semiconductors estimated after segregating the transformer, inductor and filter losses.
- Efficiency can be improved by improving transformer design and reducing switching frequency for reduced turn-off losses.

Hardware prototype of the AC/DC DAB converter

SiC Bi-Directional FET (BiDFET) packaging: 1200V, 50A half-bridge module



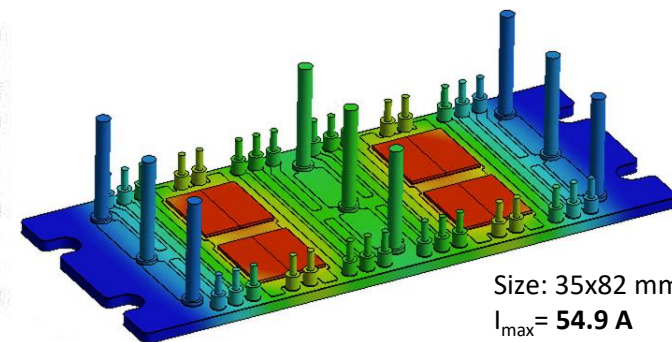
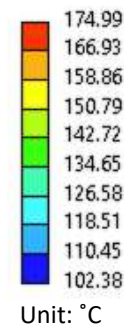
Half-bridge module schematic.



Half-bridge module packaging layout.



Fabricated half-bridge module.

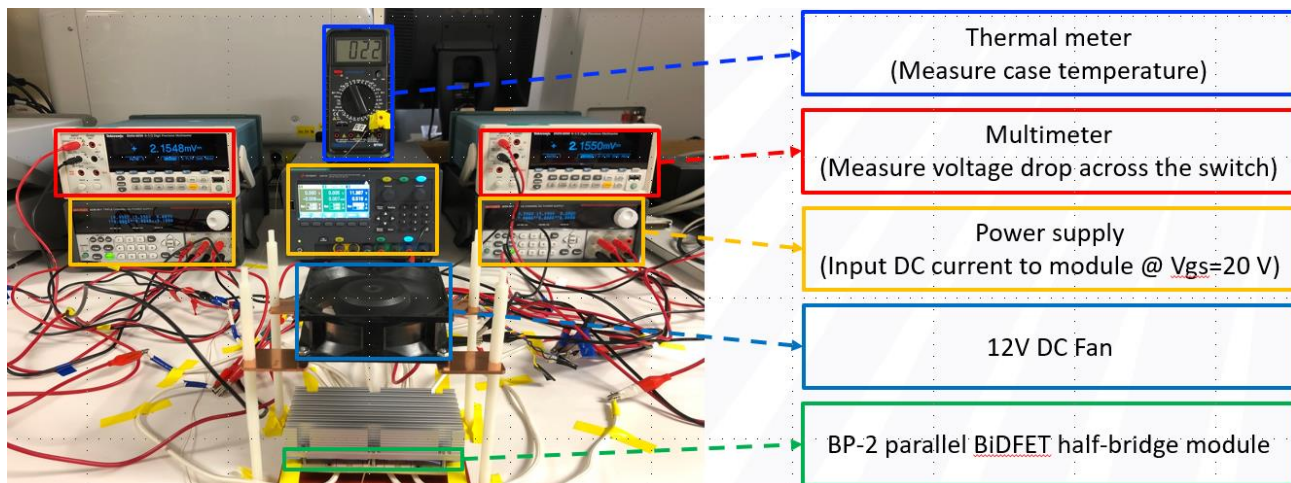


Size: 35x82 mm
 $I_{max} = 54.9 \text{ A}$
 $P_{max} = 226.8 \text{ W}$

Half-bridge module thermal simulation
($h_{coeff} = 750 \text{ W/m}^2\text{K}$ and $T_a = 25^\circ \text{C}$).

- The designed Half-Bridge Module contains two BiDFETs in Parallel per switch to enhance current and power handling capability.
- The package is designed symmetrically to allow for easy installation in the converter.

SiC Bi-Directional FET (BiDFET) packaging: 1200V, 50A half-bridge module

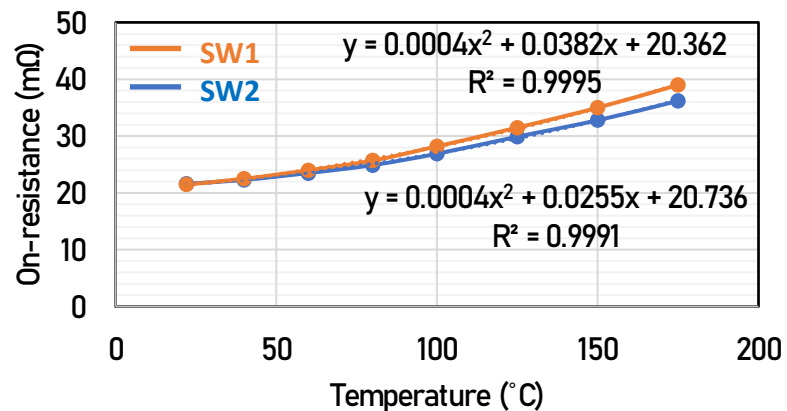


Thermal meter (Measure case temperature)
Multimeter (Measure voltage drop across the switch)
Power supply (Input DC current to module @ $V_{gs}=20$ V)
12V DC Fan
BP-2 parallel BiDFET half-bridge module

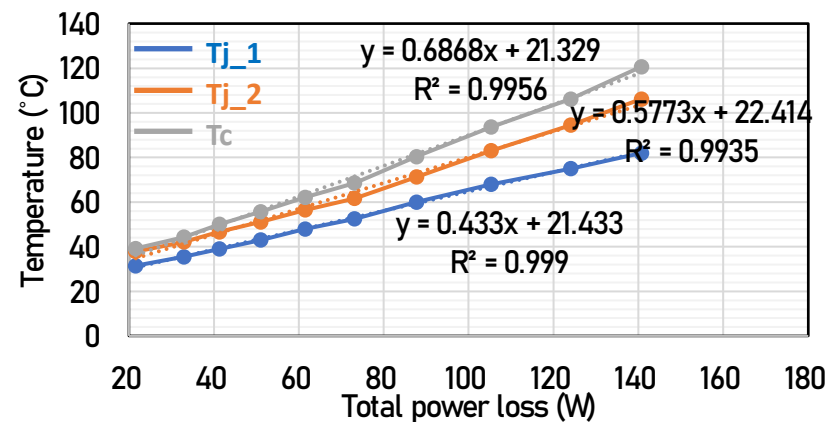
Half-bridge module experimental thermal characterization testbench.

I (A)	V1 (V)	V2 (V)	Ron_1 (mΩ)	Ron_2 (mΩ)	P1 (W)	P2 (W)	P_total (W)	Tc (°C)	Tj_1 (°C)	Tj_2 (°C)
22	0.49	0.49	22.2	22.3	10.8	10.8	21.6	31.5	37.9	39.2
27	0.61	0.61	22.5	22.7	16.4	16.5	32.9	35.5	42.1	44.3
30	0.69	0.69	22.8	23.1	20.6	20.8	41.3	39	46.7	50.0
33	0.77	0.78	23.1	23.5	25.4	25.7	51.1	43	51.1	55.7
36	0.85	0.86	23.5	23.9	30.5	31.0	61.5	48	56.5	62.2
39	0.93	0.95	23.9	24.4	36.2	37.0	73.1	52.5	61.7	68.6
42	1.03	1.06	24.6	25.3	43.2	44.5	87.7	60	71.3	80.4
45	1.15	1.19	25.6	26.4	51.8	53.6	105.3	68	83.0	93.7
48	1.27	1.32	26.5	27.6	60.8	63.2	124.1	75	94.5	106.2
50	1.38	1.45	27.6	29.0	68.6	72.1	140.7	82	106.2	120.7

Experimental thermal characterization testdata.



Ron vs temperature

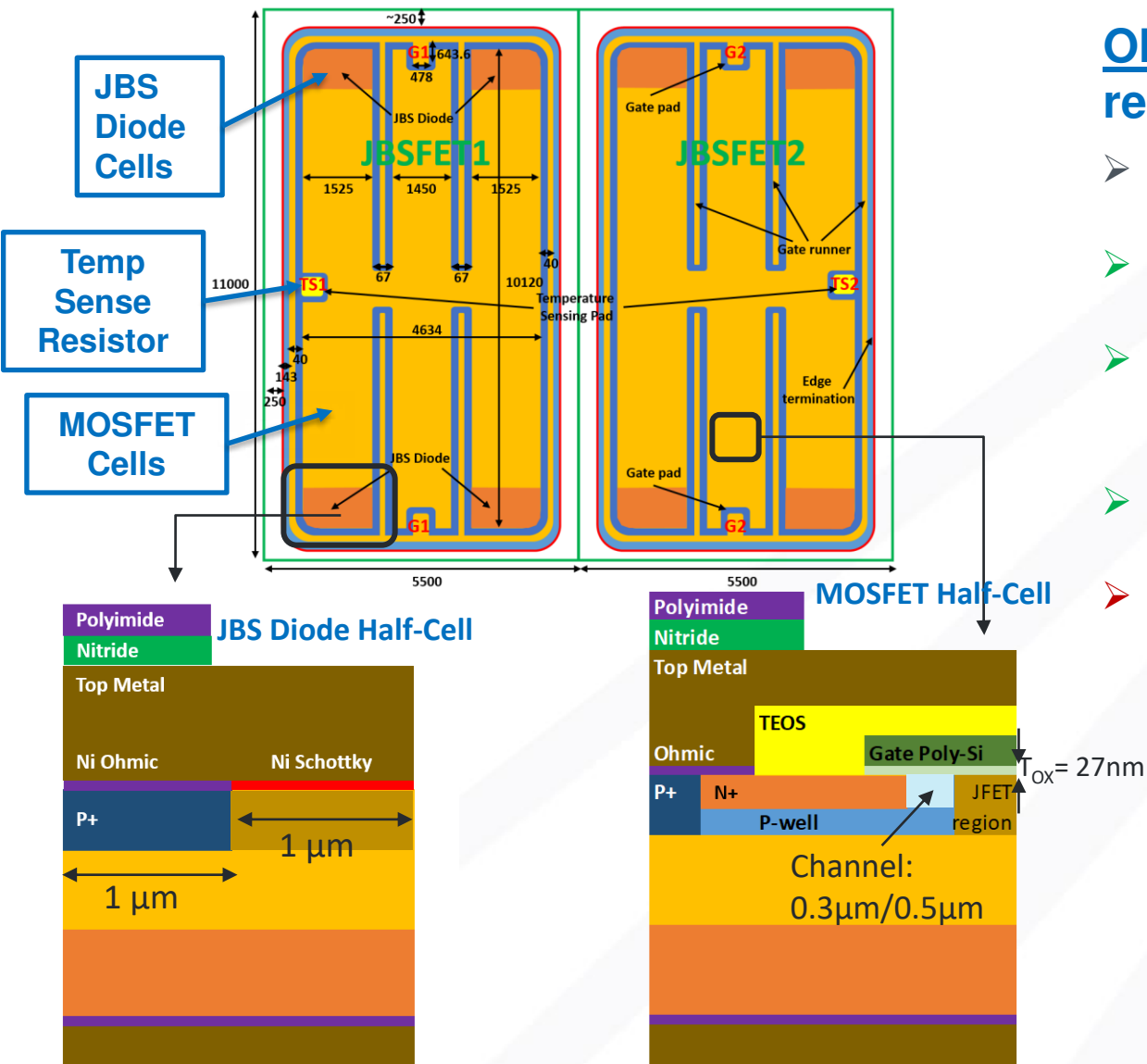


Power loss vs temperature

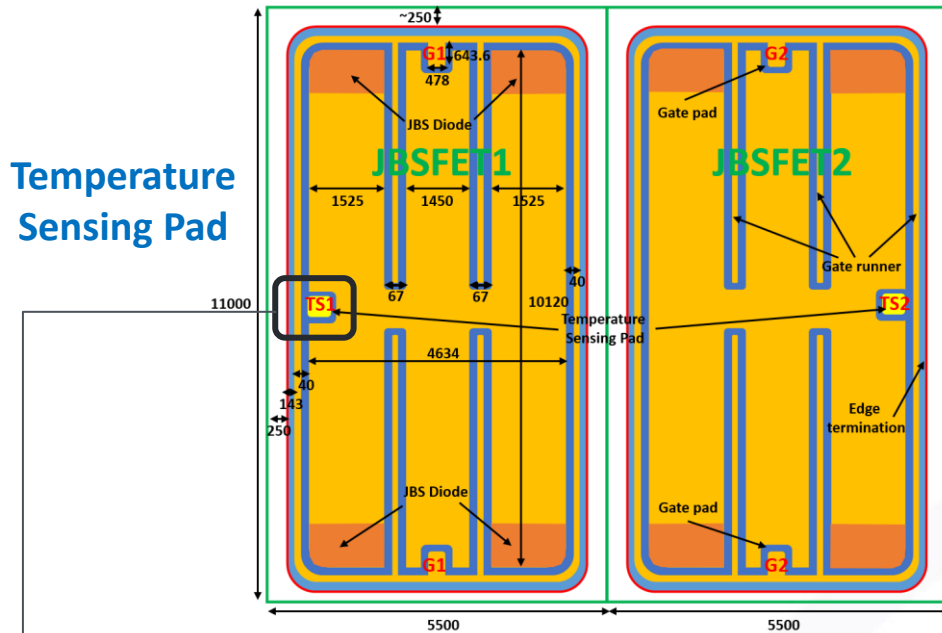
Gen-2 BiDFET: Chip Design

Objective: Improved design with 2x lower specific on-resistance for the same die size.

- Gen-1 BiDFET, with on-resistance of 50 mΩ, has JBS diode integrated within MOSFET cells.
- **Gen-2 BiDFET, with on-resistance of 26 mΩ, has JBS diode and MOSFET in separate parts of the JBSFET chip.**
- **Gen-2 BiDFET On-Resistance further reduction achieved by reducing gate oxide thickness from 55 to 27 nm and reducing channel length from 0.5 μm to 0.3 μm.**
- **Higher ohmic contact anneal temperature used to further reduce specific on-resistance.**
- **New BP-2 BiDFET Design has same active area and chip size as the BP-1 BiDFET.**
 - **JBS Diode Active Area = 0.045 cm²**
 - **MOSFET Active Area = 0.405 cm²**
 - **MOSFET $R_{on,sp} = 5.3 \text{ m}\Omega\text{-cm}^2$**
 - **MOSFET $R_{on} = 13 \text{ m}\Omega$**
 - **BP-2 BiDFET $R_{on} = 26 \text{ m}\Omega$**
 - **BP-2 BiDFET $I_{on} = 25 \text{ A}$**
 - **BP-2 BiDFET $V_{on} = 0.65 \text{ V @ } 25 \text{ A}$**

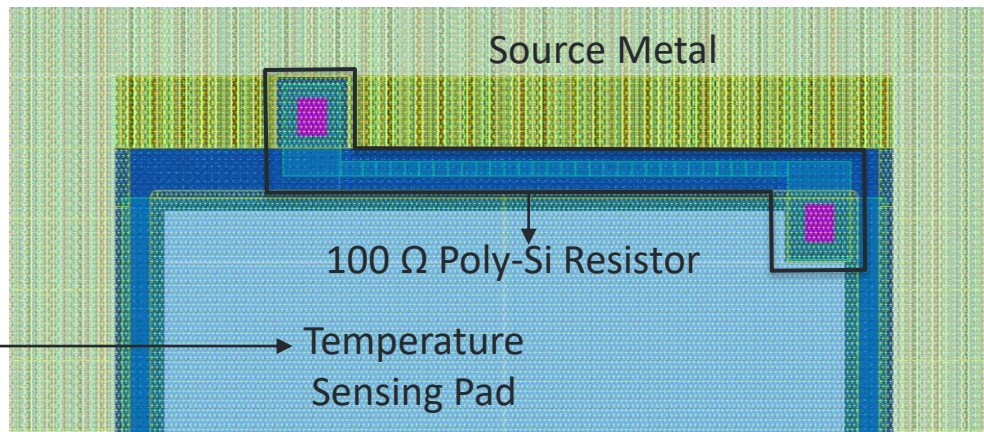


Gen-2 BiDFET: Temperature Sensor



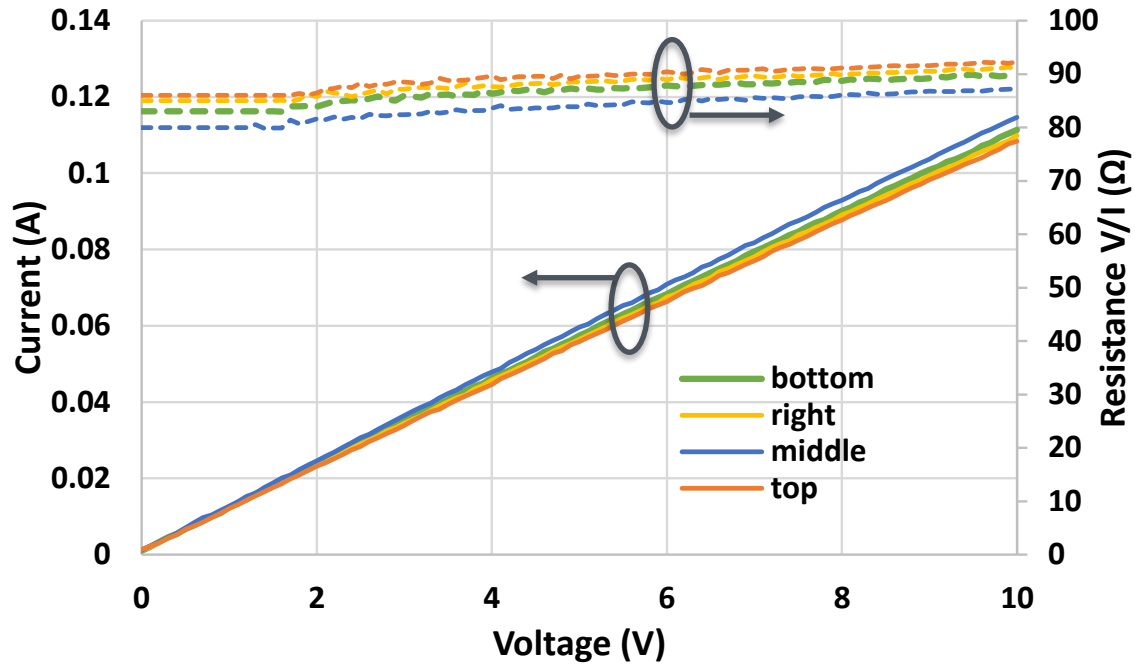
New feature created in Gen-2 BiDFET: On-Chip Temperature Sensing Capability

- **Makes use of Silicided Polysilicon Gate Electrode Layer**
- **No additional processing steps required**
- **Silicided Polysilicon Sheet Resistance: 3 Ω /square**
- **100 Ω Poly-Si resistor integrated on-chip to allow BiDFET device temperature monitoring**

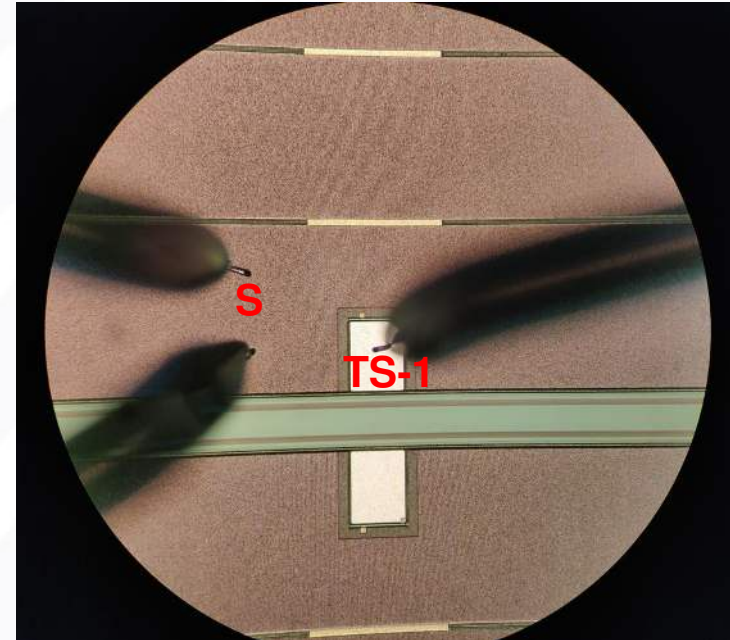


Temperature Sense Resistor: Uniformity

Sense Resistor Room Temperature Data



Wafer Position	R
Bottom	90 Ω
Right	91 Ω
Middle	87 Ω
Top	92 Ω



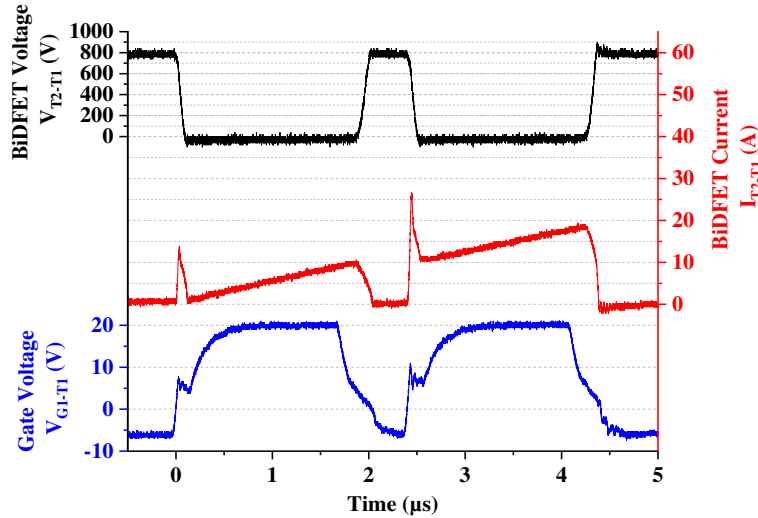
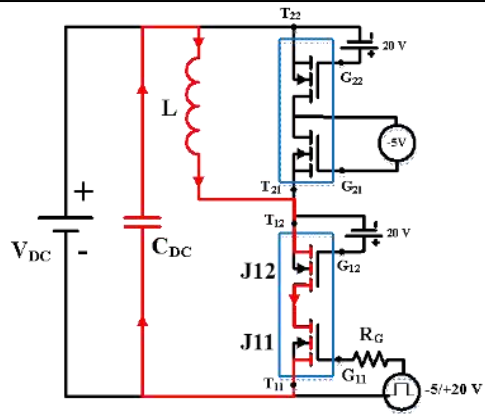
- Measured Temperature Sense Resistance @ RT = 90 Ω
- Matches design value of ~100 Ω
- Achieved project goal



The 1.2 kV BiDFET Switch: Switching Performance

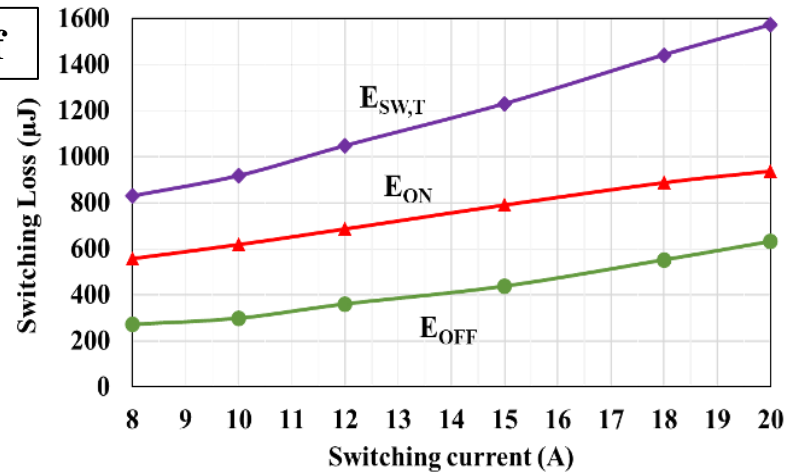
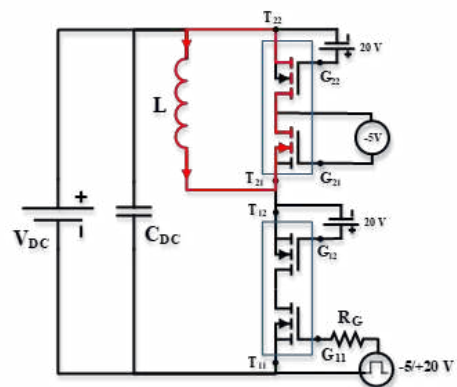
Test Conditions: $V_{DC} = 800\text{ V}$, $I_{T_2T_1} = 8\text{-}20\text{ A}$, Case Temperatures: $25\text{ }^\circ\text{C}$, Gate resistances = $10\text{ }\Omega$
 LS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5/20\text{ V}$, $V_{G_2T_2} = 20\text{ V}$), HS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5\text{ V}$, $V_{G_2T_2} = 20\text{ V}$)

Current Flow Schematics: With Low-side BiDFET G_{11} On



I_{ON} (A)	E_{ON} (μJ)	E_{OFF} (μJ)	$E_{SW,T}$ (μJ)	$E_{SW,T}$ Norm.
8	559	271	830	0.9
10	620	298	918	1.0
12	688	360	1048	1.14
15	792	438	1230	1.34
18	889	553	1442	1.57
20	939	633	1572	1.71

With Low-side BiDFET G_{11} Off



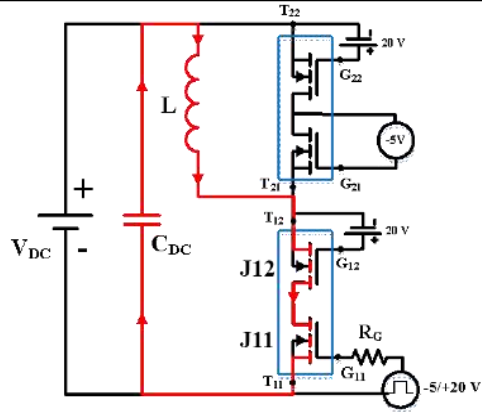
The BiDFET switching losses increase by a factor of 1.71x when I_{ON} rises from 10 to 20 A.

The BiDFET exhibits a current overshoot during turn-on transitions due to output capacitance of HS switch.

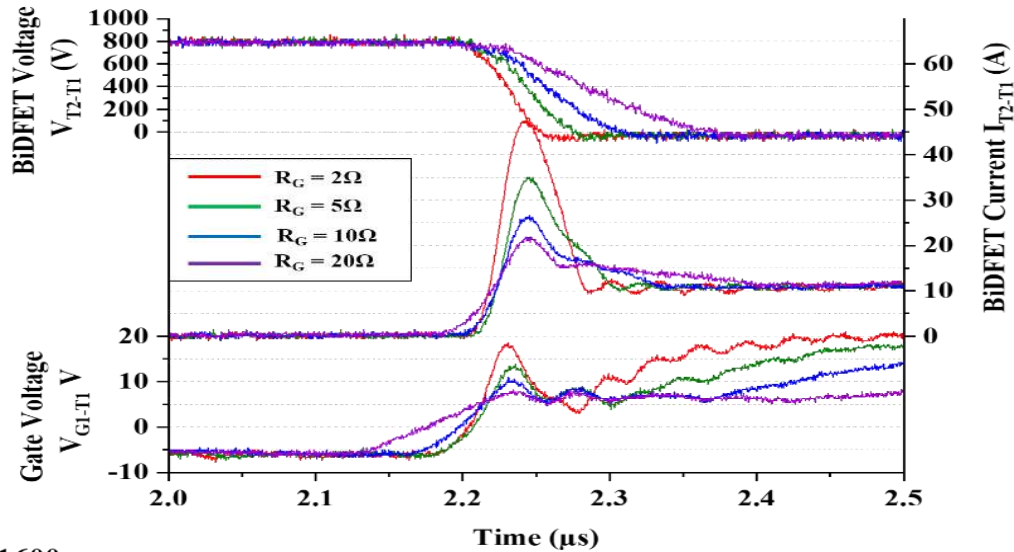
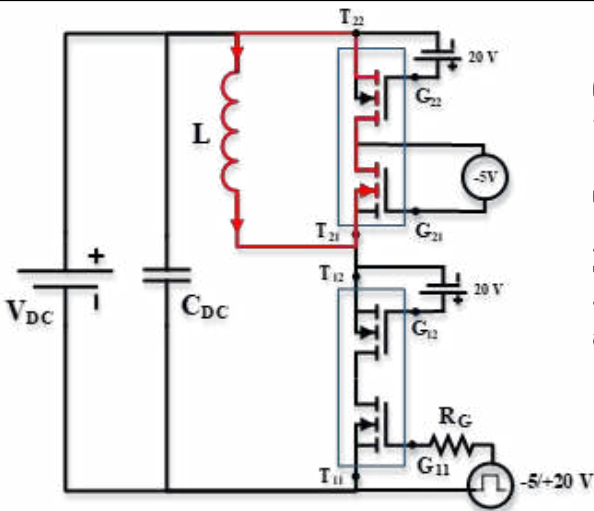
The 1.2 kV BiDFET Switch: Switching Performance

Test Conditions: $V_{DC} = 800\text{ V}$, $I_{T_2T_1} = 10\text{ A}$, Case Temperatures: $25\text{ }^\circ\text{C}$, Gate resistances = 2-20 Ω
 LS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5/20\text{ V}$, $V_{G_2T_2} = 20\text{ V}$), HS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5\text{ V}$, $V_{G_2T_2} = 20\text{ V}$)

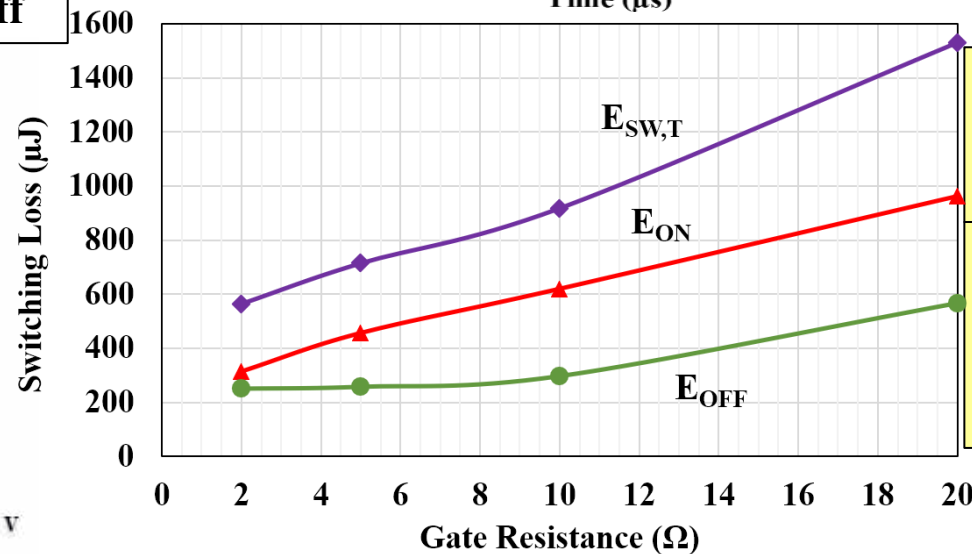
Current Flow Schematics: With Low-side BiDFET G_{11} On



With Low-side BiDFET G_{11} Off



R_G (Ω)	E_{ON} (μJ)	E_{OFF} (μJ)	$E_{SW,T}$ (μJ)	$E_{SW,T}$ Norm.
2	313	252	565	0.62
5	456	259	715	0.78
10	620	298	918	1.00
20	964	566	1530	1.67



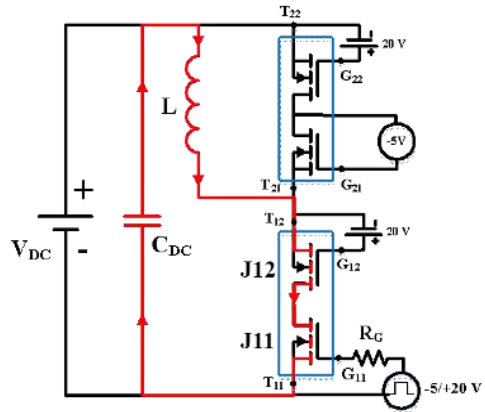
The BiDFET switching losses increase with gate resistance due to increased switching transition time.

Increased gate resistance reduces gate current leading to a slow transient (reduced dV/dt). The slow transients result in a reduced current overshoot at turn-on.

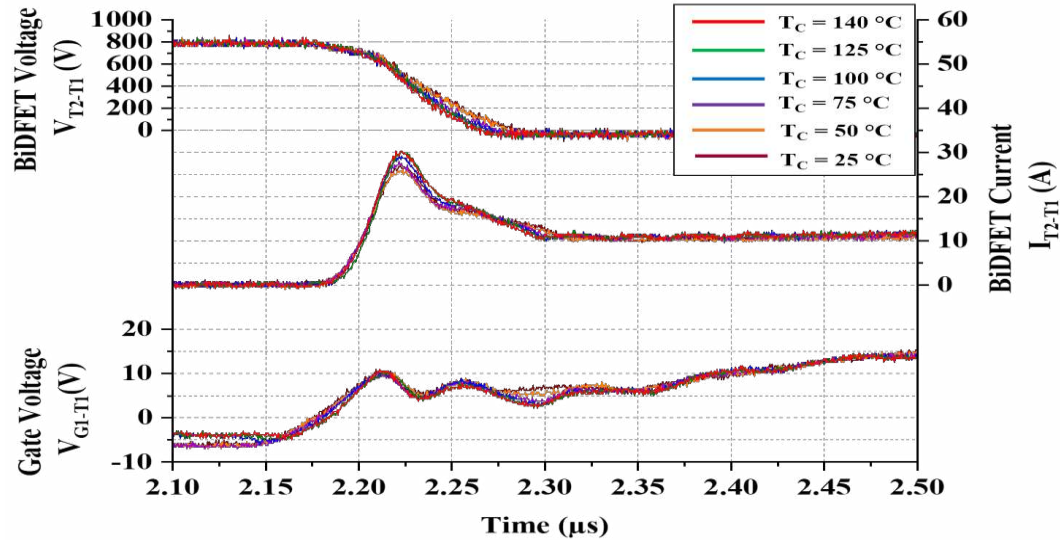
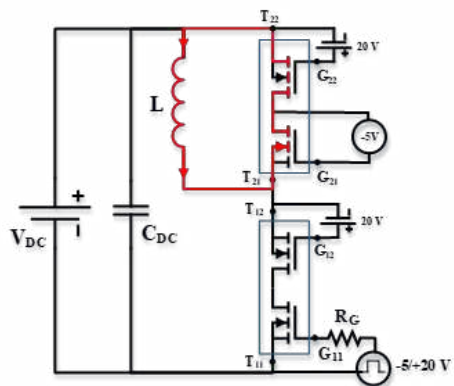
The 1.2 kV BiDFET Switch: Switching Performance – Loss vs Case Temperature

Test Conditions: $V_{DC} = 800\text{ V}$, $I_{T_2T_1} = 10\text{ A}$, Case Temperatures: 25-140 °C, Gate resistances = 10 Ω
 LS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5/20\text{ V}$, $V_{G_2T_2} = 20\text{ V}$), HS Switch: 1.2 kV BiDFET ($V_{G_1T_1} = -5\text{ V}$, $V_{G_2T_2} = 20\text{ V}$)

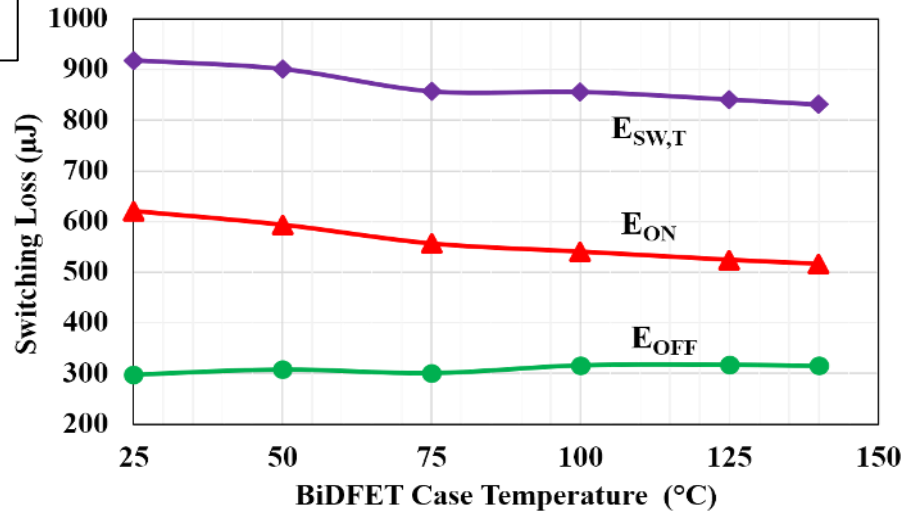
Current Flow Schematics: With Low-side BiDFET G_{11} On



With Low-side BiDFET G_{11} Off



T_C (°C)	E_{ON} (μJ)	E_{OFF} (μJ)	$E_{SW,T}$ (μJ)	$E_{SW,T}$ Norm.
25	620	298	918	1
50	593	308	901	0.96
75	556	301	857	0.9
100	540	316	856	0.87
125	524	317	841	0.85
140	516	315	831	0.83



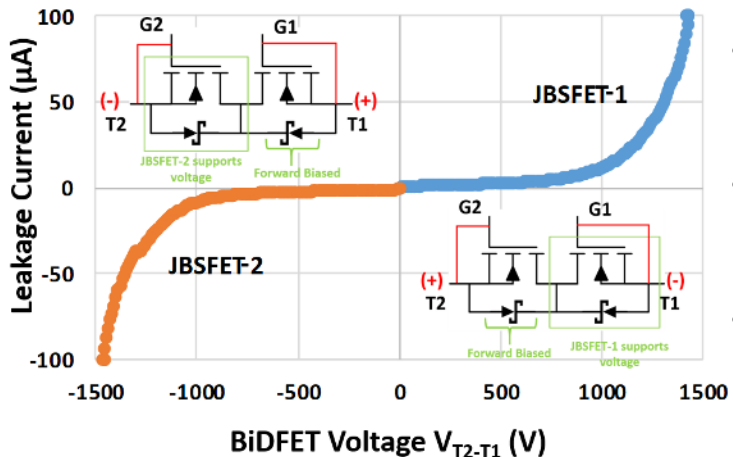
Reduced output capacitance of the high-side switch results in reduction of switching loss with case temperature.

The BiDFET switching losses decrease by 17% as case temperature increases from 25 °C to 140 °C.

Peak currents at turn-on exhibit small reduction with increasing case temperature.

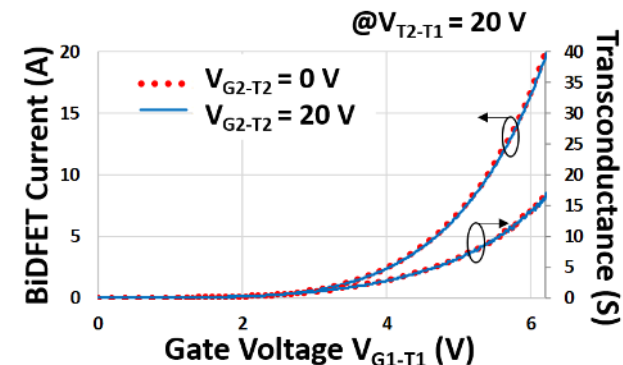
The 1.2 kV BiDFET Switch: Static Characterization

BiDFET blocking characteristics:



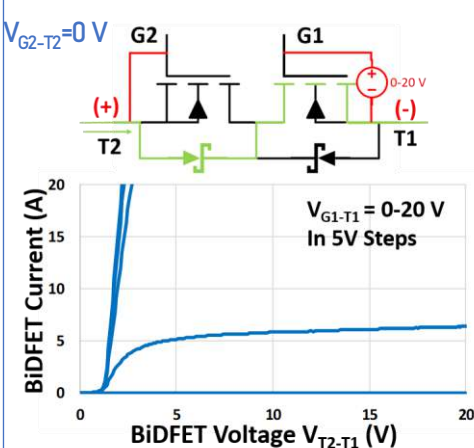
- In 1st quadrant: $V_{G1-T1}=V_{G2-T2}=0$ V, $V_{T2-T1}>0$ V, V_{T2-T1} supported by JBSFET-1.
- In 3rd quadrant: $V_{G1-T1}=V_{G2-T2}=0$ V, $V_{T2-T1}<0$ V, V_{T2-T1} supported by JBSFET-2.
- BV @ 100 µA > **1400 V** in both 1st and 3rd quadrants.

BiDFET transfer characteristics:

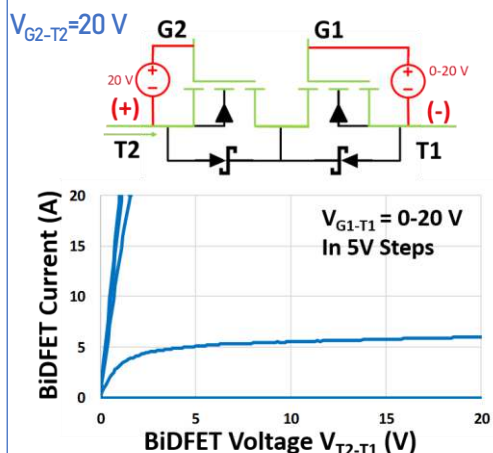


- Conduction through JBSFET-1 channel for both cases.
- V_{th} @ $V_{T2-T1}=20$ V, $I_{T2-T1}=10$ mA was **1.35 V**.
- G_m @ $V_{T2-T1}=20$ V, $I_{T2-T1}=20$ A was **17 S**.

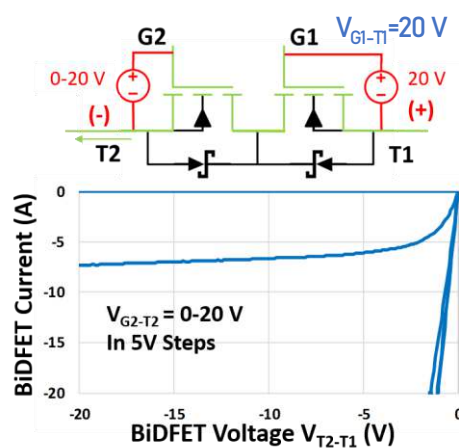
BiDFET output characteristics:



- Conduction through series JBS diode.
- Knee Voltage = **1.2 V**.

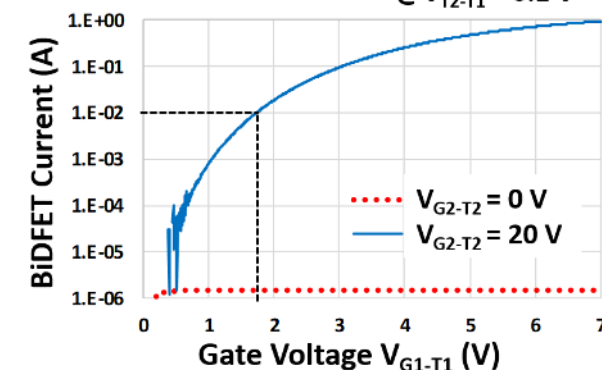


- Output characteristics in 1st quadrant for $V_{G2-T2}=20$ V.
- R_{on} @ $I_{T2-T1}=10$ A and $V_{G1-T1}=20$ V is **50 mΩ**.



- Output characteristics in 3rd quadrant for $V_{G1-T1}=20$ V.
- R_{on} @ $I_{T2-T1}=-10$ A and $V_{G2-T2}=20$ V is **50 mΩ**.

BiDFET transfer characteristics:



- Conduction through JBSFET-1 & JBSFET-2 channels for $V_{G2-T2}=20$ V case.
- No conduction for $V_{G2-T2}=0$ V case, because 0.1 V on T2 is not enough to forward bias internal JBS diode of JBSFET-2.
- V_{th} @ $V_{T2-T1}=0.1$ V, $I_{T2-T1}=10$ mA was **1.73 V**.

Acknowledgments:

- Prof. Baliga – SiC BiDFET device
- Prof. Hopkins – Advanced packaging of SiC BiDFET device
- **Graduate Students:**
- Device: Aditi Agarwal, Kijeong Han, Ajit Kanale
- Advanced Packaging: Tzu-Hsuan Cheng
- PV converter: Ramandeep Narwal
- Magnetics: Isaac Wong, Sagar Rastogi
- **Post-Doc:**
- PV Converter Applications: Suyash Shah
- **Device Manufacturing:**
- X-FAB Foundry: Voshadhi Amarsinghe, John Ransom
- **Sponsor: DOE SETO [Grant DEEE0008345]; NASA**