



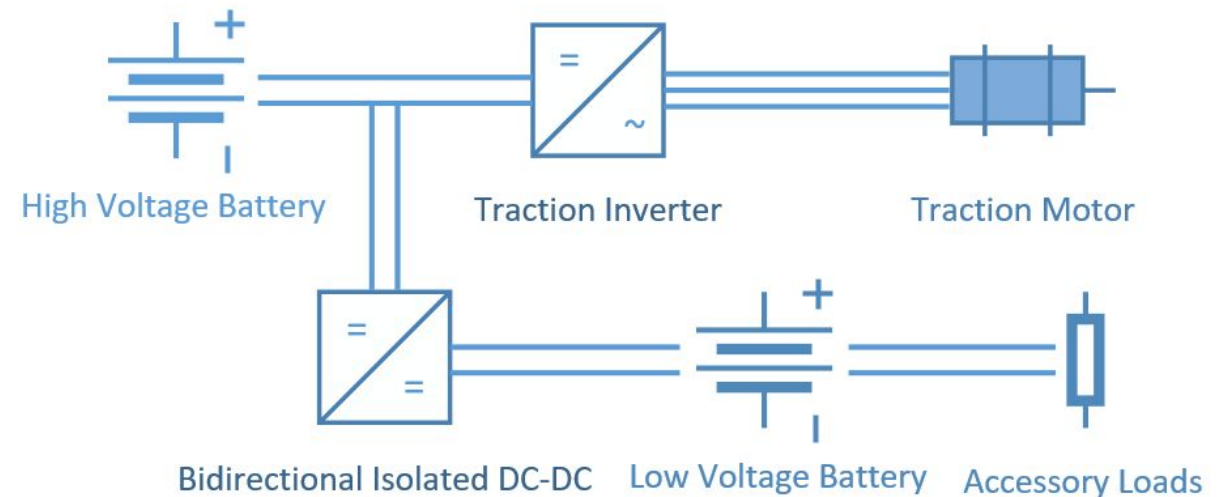
Bidirectional Shared-Switch DC-DC
Converter for Electric Vehicle Applications

Michael Kercher, PhD Student

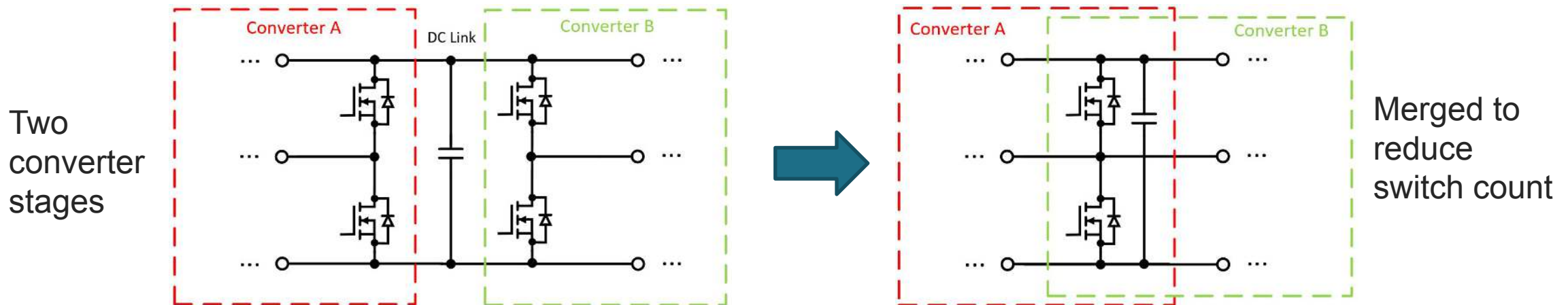
FREEDM Symposium

April 3, 2024

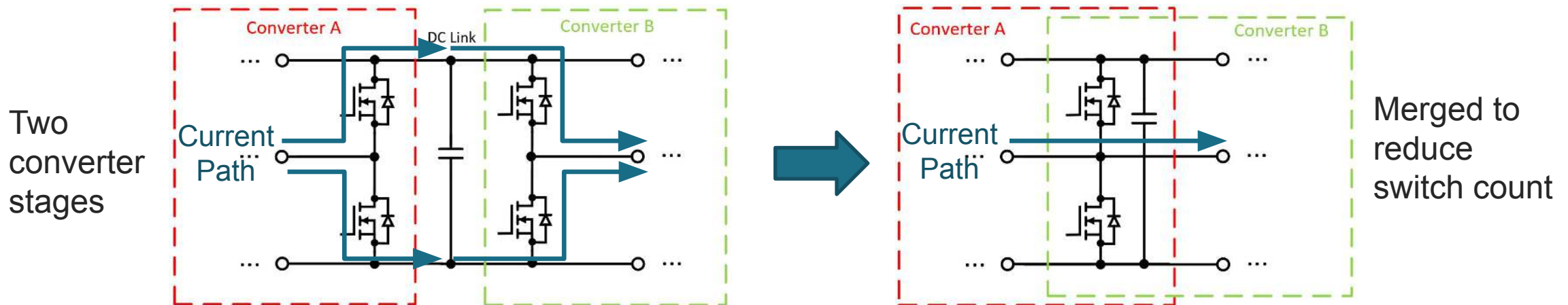
- Energy from the main battery pack is consumed by:
 - Traction drive system
 - Accessory loads via low voltage subsystem, such as lighting, climate control, radio, etc.
- DC-DC converter connects high and low voltage systems with galvanic isolation
 - Typical size:
 - 2-3 kW (passenger)
 - 5-10 kW + (heavy duty)



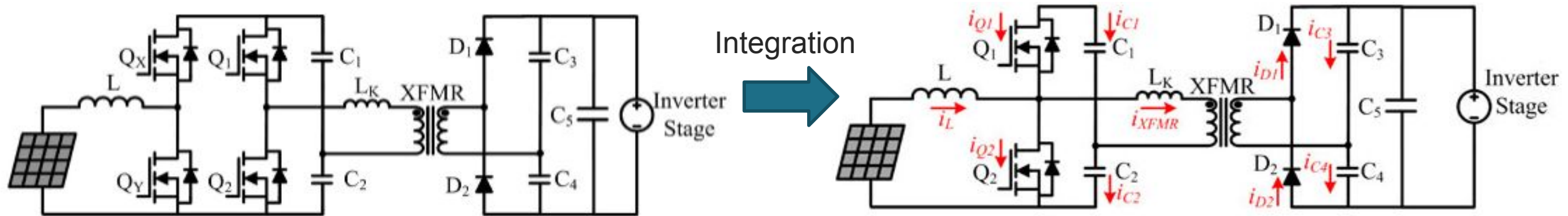
- Increase efficiency - improves battery life, reduces cooling needs
- Increase density - less mass, easier packaging
- Reduce cost - improved value for manufacturer and consumer
- *The proposed “Shared-Switch Converter” can achieve all 3*
 - One set of switches performs functions for two converter stages
 - Lower parts count means lower size, cost, and losses



- Benefits:
 - Reduced parts count – smaller, lighter, cheaper
 - Fewer switches to generate switching losses
 - More direct current path reduces conduction loss
- Challenges, gaps in prior art:
 - Gating generation to ensure proper operation of both converters under all conditions – unique to the specific topology
 - Modeling for shared-switch topologies, especially if converters operate in different modes (CCM vs. DCM, etc.)
 - Hardware design: component sizing, minimization of parasitic effects



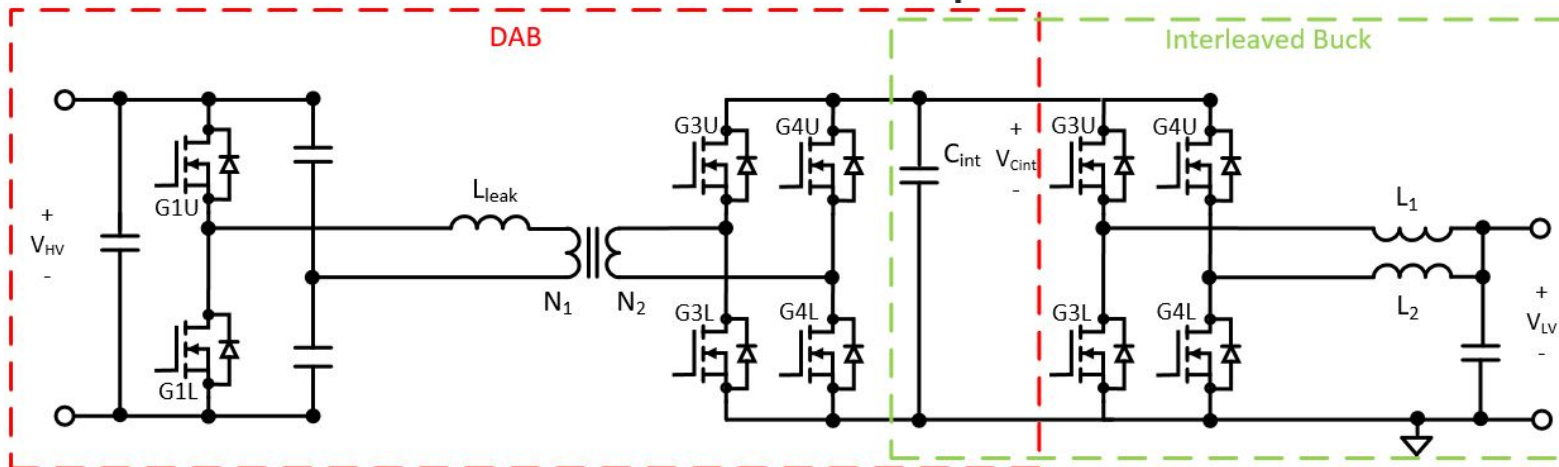
- Numerous examples of integrated topologies in literature
- Boost + Series Resonant Converter:



- Allows resonant stage to operate in efficient DCX mode across varying input voltage from photovoltaic array
- Number of active switches reduced by 50% vs. two stage converter
- Minimum 96.8% efficiency across voltage range vs. 90% for series resonant only

- Examples from literature show:
 - Improved efficiency across varying operating conditions
 - Successful reduction of active switch and filter element requirements
 - Lower cost and higher power density vs. traditional topologies
- Research objectives:
 - Increased power capability for heavy vehicle applications
 - Broader range of voltage conversion ratios to account for changing battery state of charge
 - Ability to maintain high efficiency at conversion ratio extremes
 - Straightforward method for modelling and controller development
 - Simplified control without coupling of controlled variables or nonlinear behavior

- EV DC-DC converter requirements:
 - Bidirectional power: LV battery bank can support HV bus under transients
 - Galvanically isolated
 - Wide voltage conversion ratio range 3:1 ($\frac{HV_{max}}{LV_{min}} : \frac{HV_{min}}{LV_{max}}$) due to changing battery state of charge
- Series-connected DAB and Interleaved Buck
 - DAB offers isolation, bidirectional power control
 - Interleaved buck adapts to changing voltage conversion ratio, allowing DAB to maintain ideal ratio for DCX operation¹



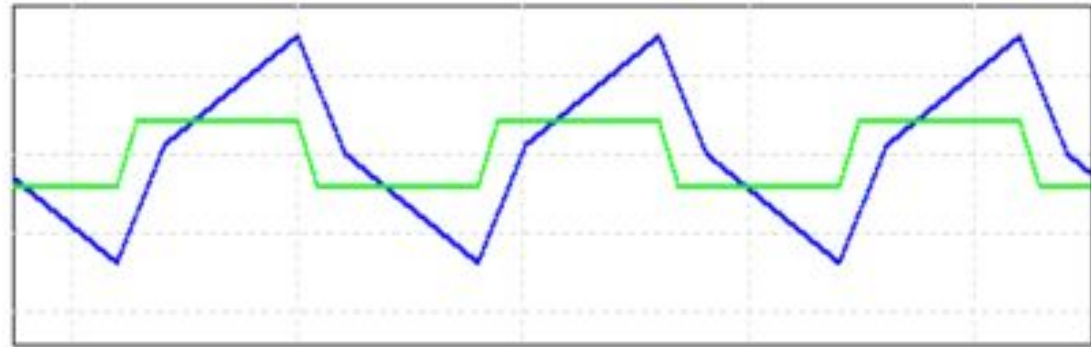
$$(1) V_{C_{int}} = \frac{1}{2} V_{HV} \frac{N_2}{N_1}$$

- DCX operation of DAB minimizes RMS winding currents, losses

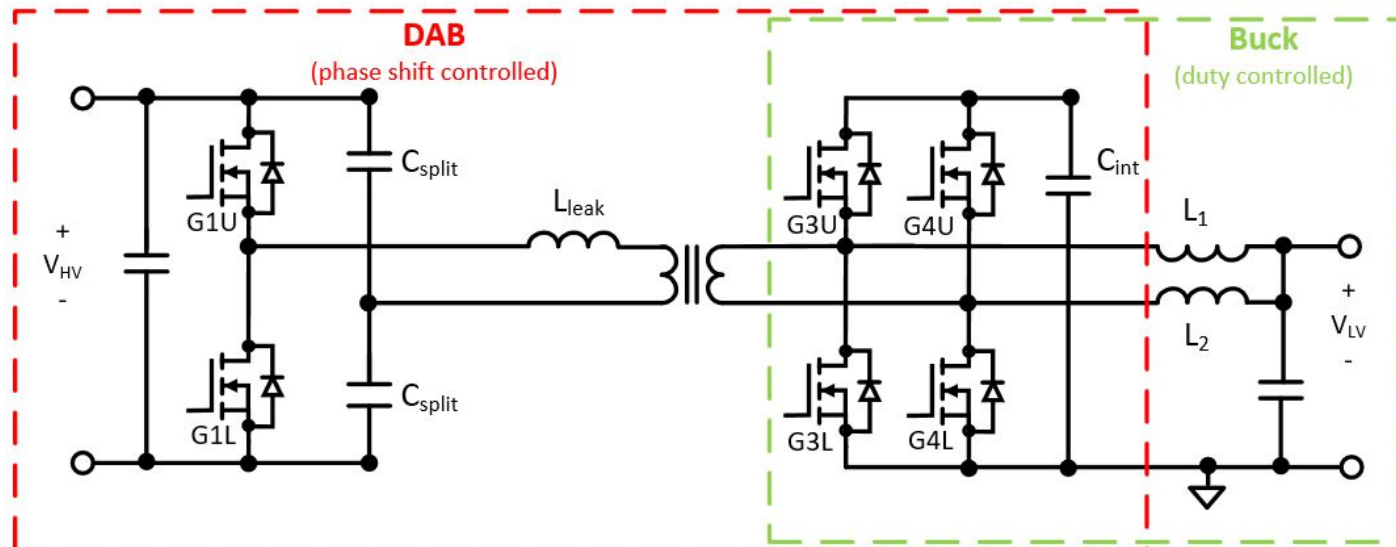
Primary Current for equal power throughput and input voltage:

Sec. voltage matched $V_{Cint} = V_{HV} \frac{N_2}{N_1}$

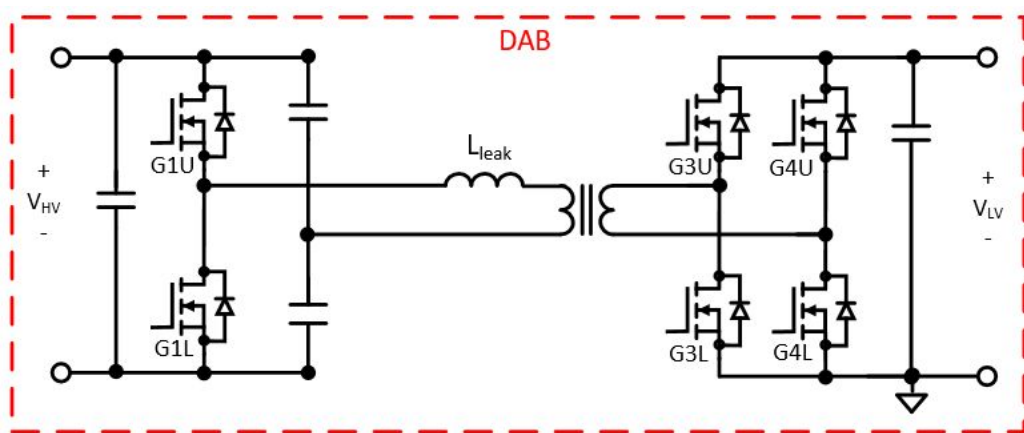
Sec. voltage mismatch $V_{Cint} \neq V_{HV} \frac{N_2}{N_1}$



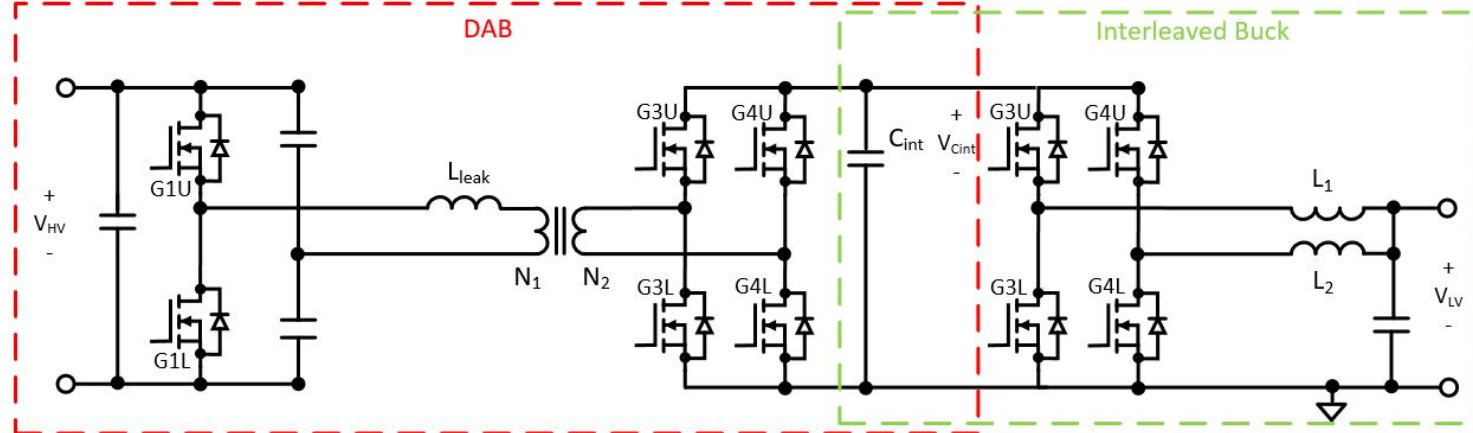
- Applying integration concept reduces switch count 40%, reduces switching and conduction losses



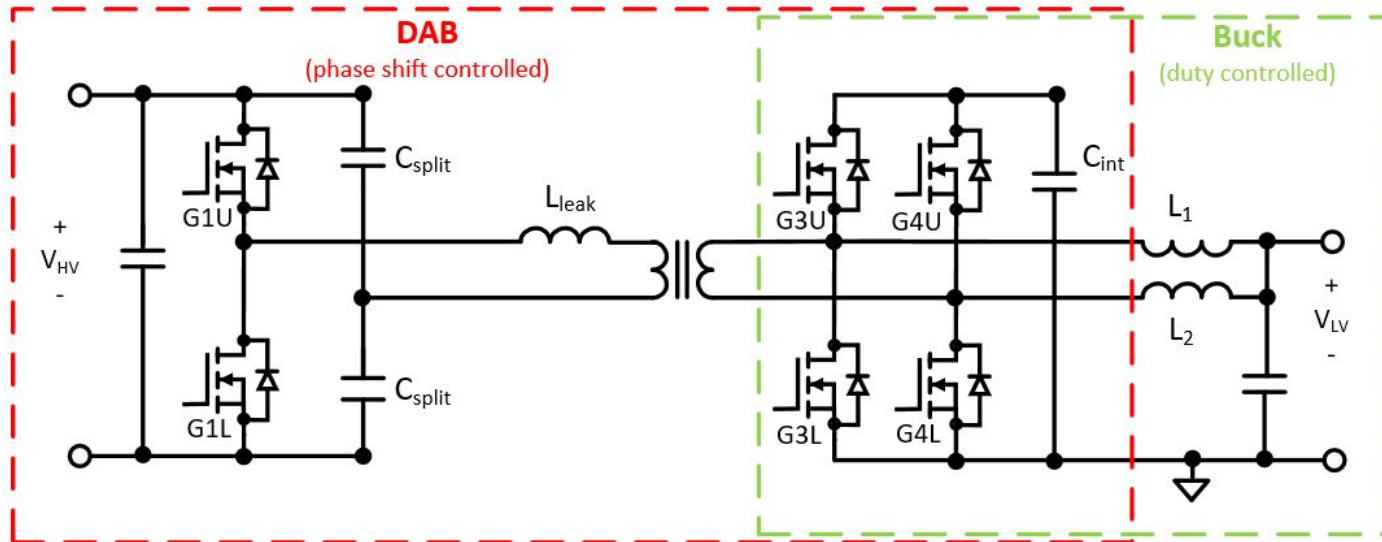
DAB

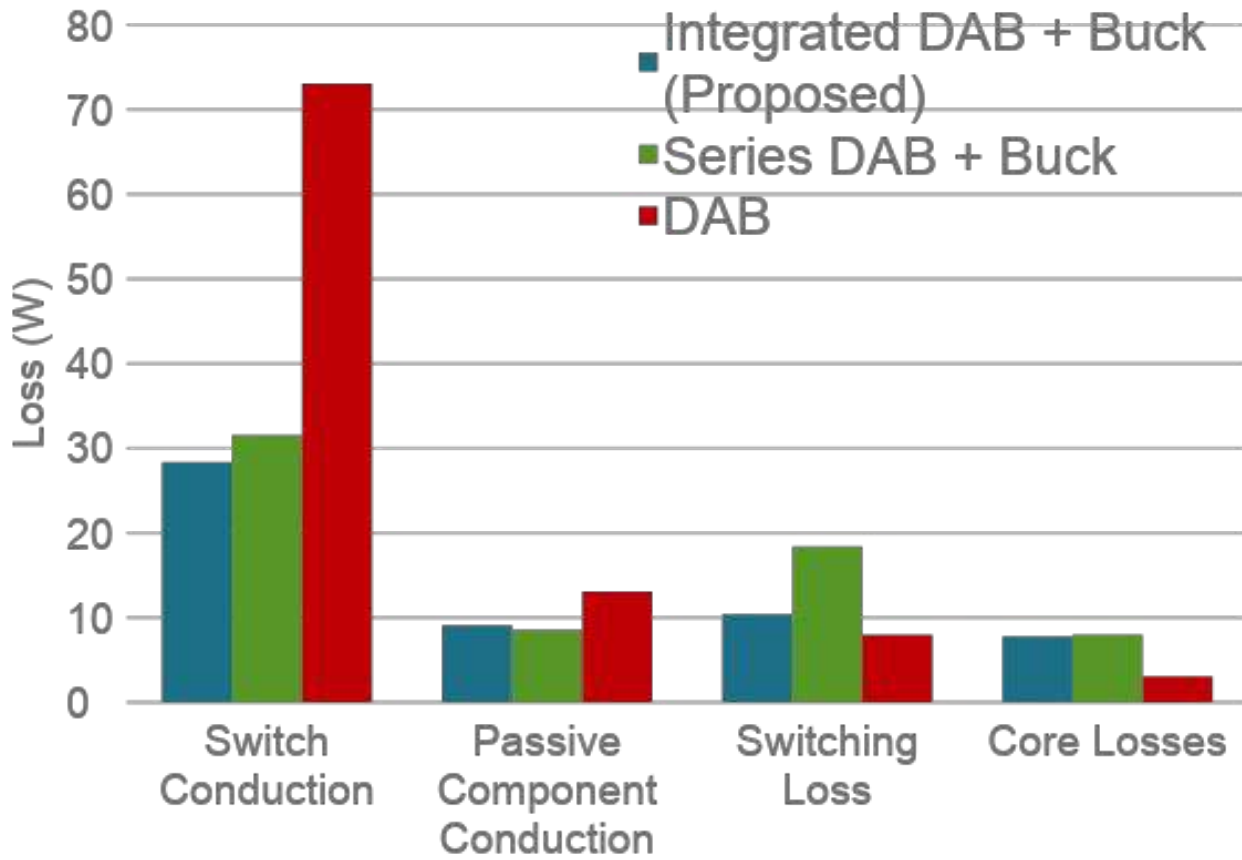


DAB + Buck

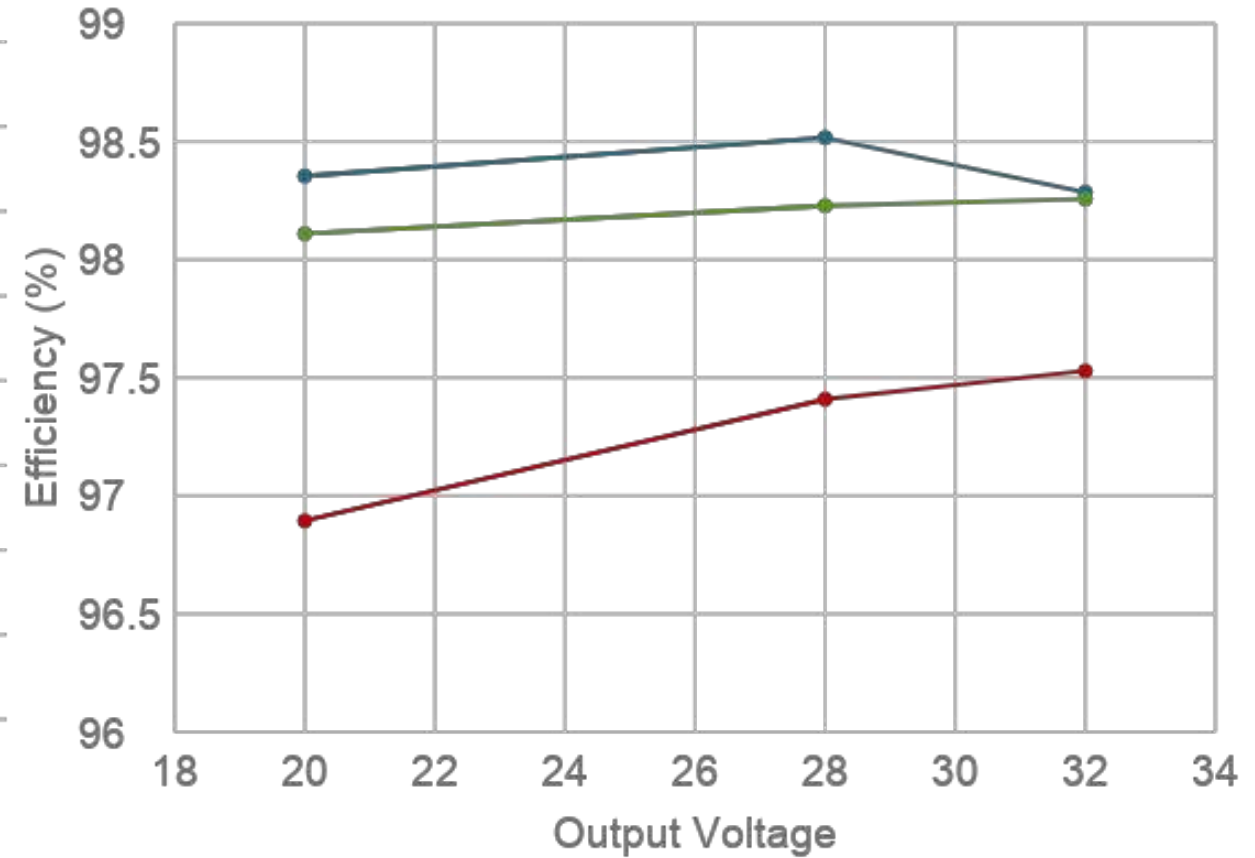


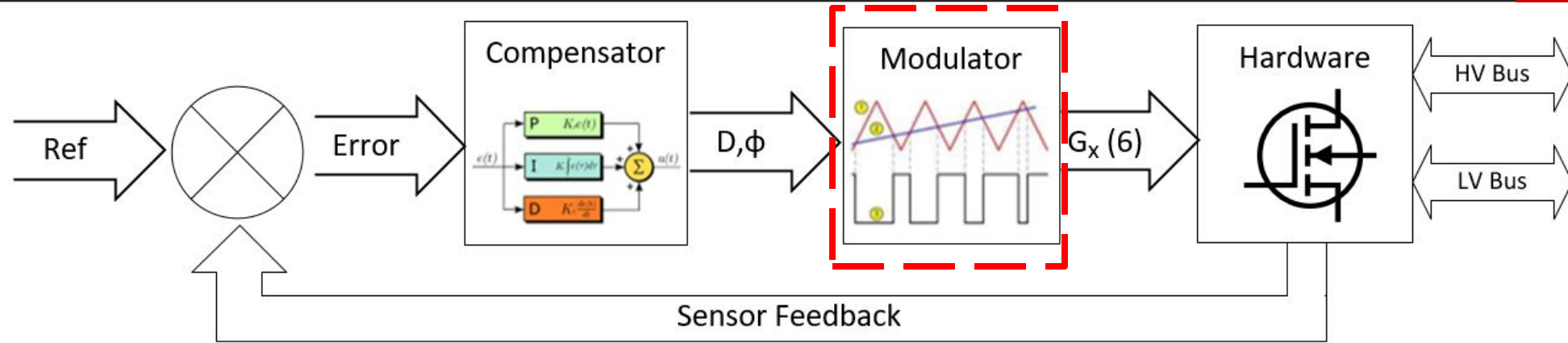
Integrated DAB + Buck





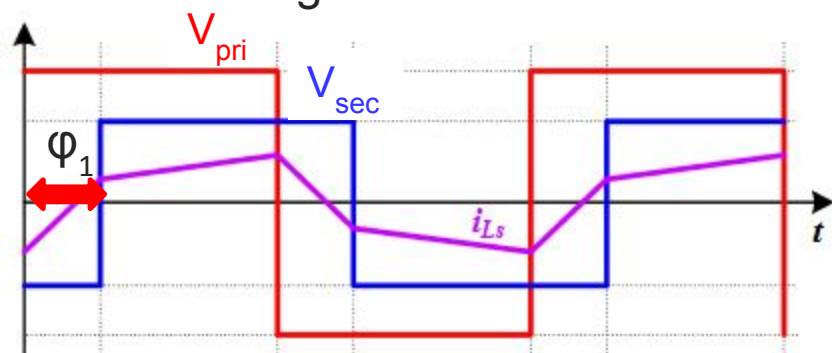
Loss Breakdown for 600V - 28V, 3.75 kW Operation



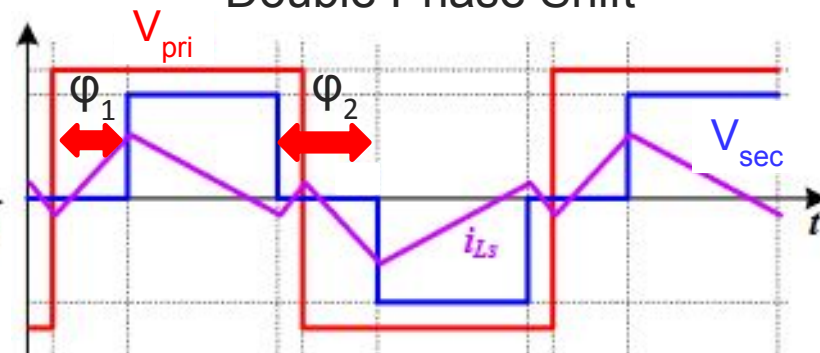


- Conventional DAB modulation: fixed 50% duty, variable phase
 - Single, Double, or Triple Phase Shift used to control power flow
 - HV bridge to LV bridge phase, phase between each full bridge leg

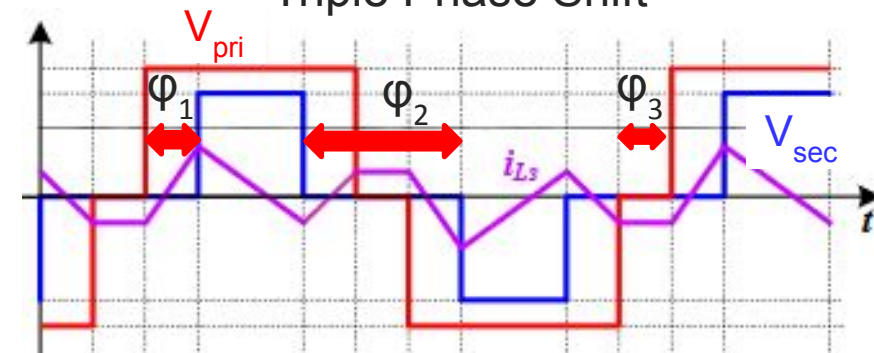
Single Phase Shift



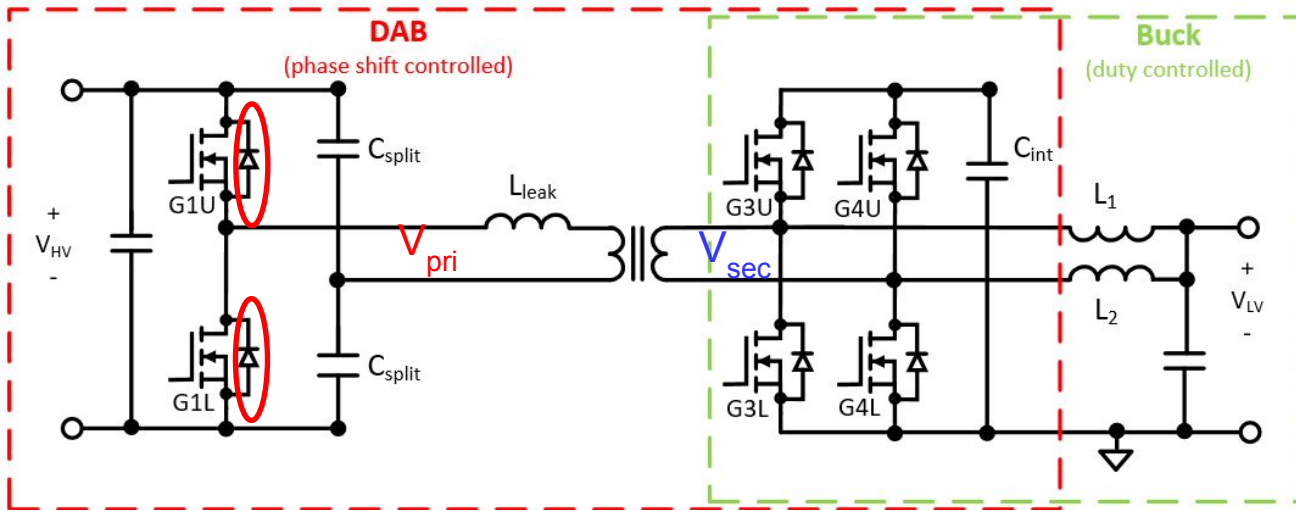
Double Phase Shift



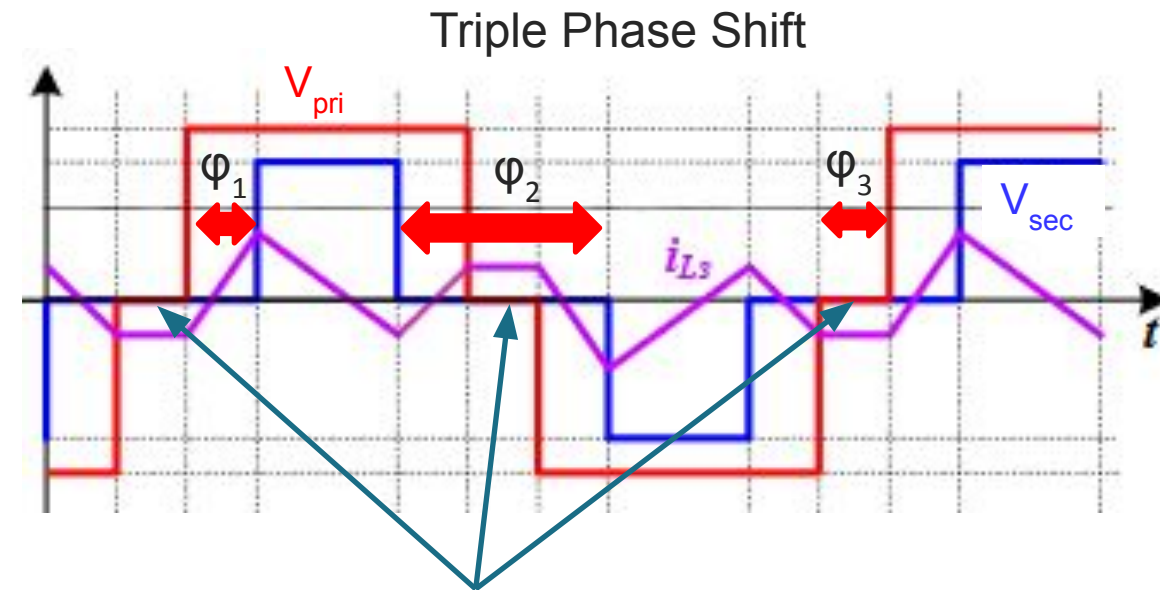
Triple Phase Shift



- Fundamental differences for proposed topology vs. traditional DAB:
 - LV Duty $\neq 50\%$ - variable according to buck converter requirements – not DAB
 - HV half bridge cannot enforce $V_{pri} = 0$ when $I_{pri} \neq 0$
- DAB and Buck interaction causes control difficulty

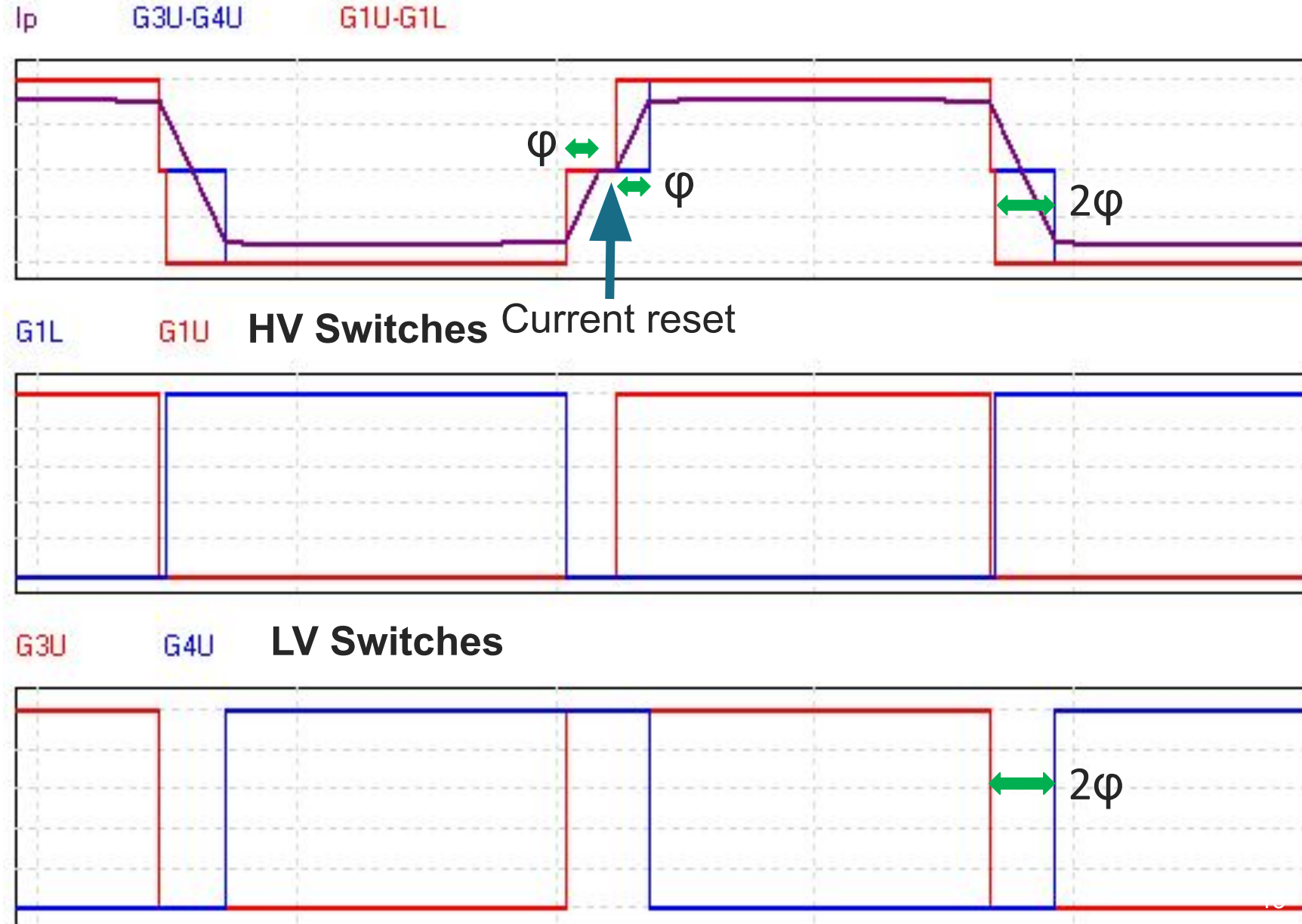


$$D_3 = D_4 = \frac{2 V_{LV} N_2}{V_{HV} N_1}$$

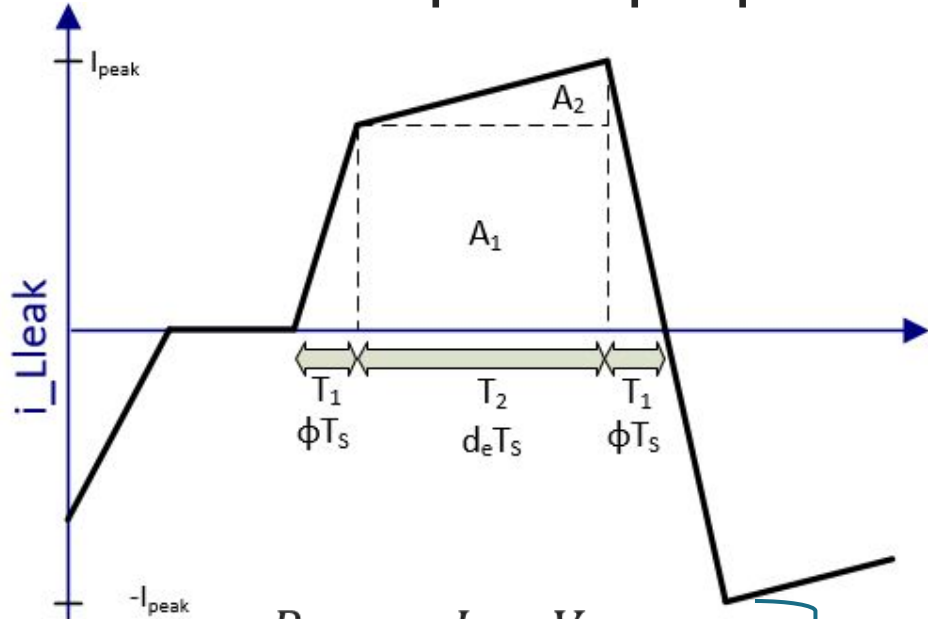


Not possible due to S1U or S1L body diode conduction

- Phase shift between LV legs provides magnetizing current reset once per period for any duty



- DAB output is proportional to new control input "Vm"

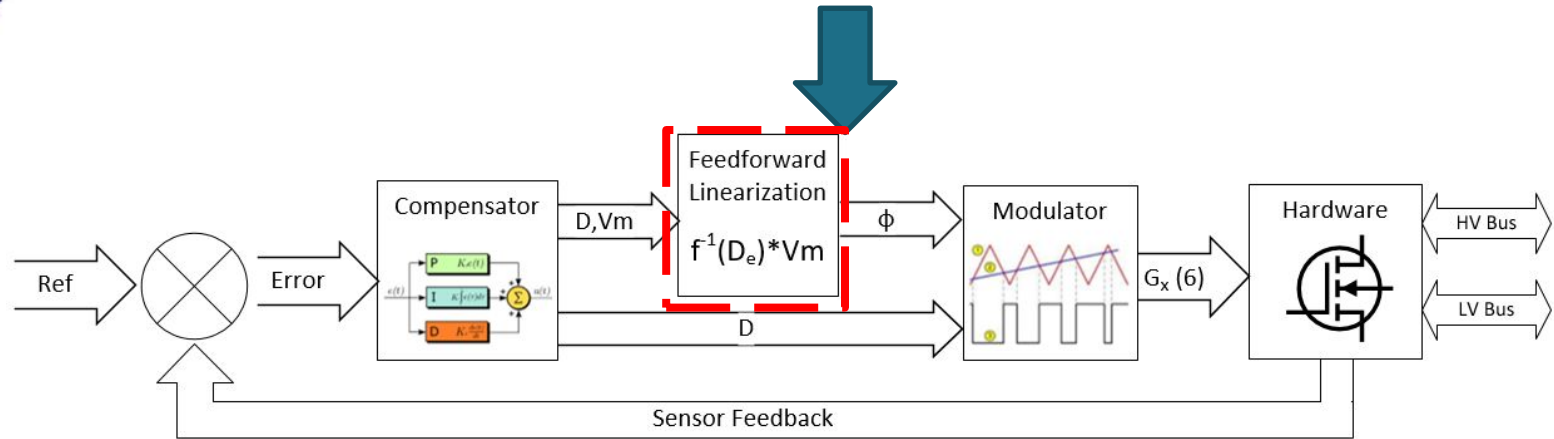
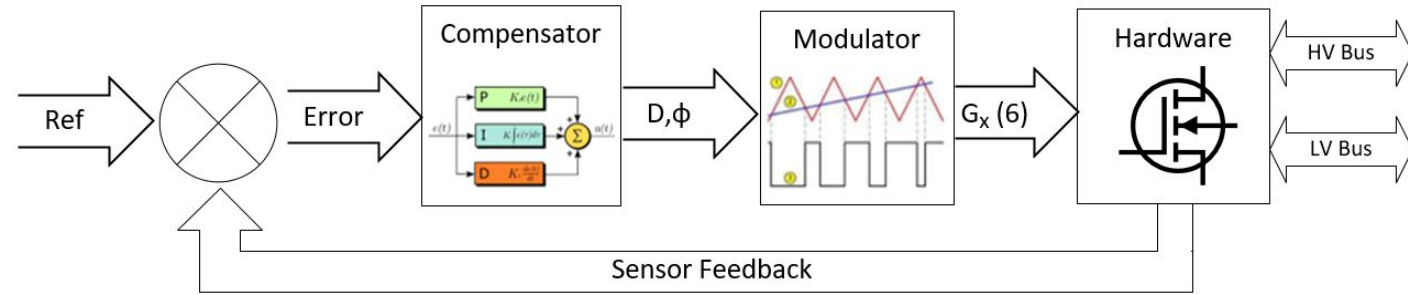


$$P_{DAB} = I_{DAB} V_{LV}$$

$$I_{DAB} = \frac{2 * (A_1 + A_2) N_1}{T_s N_2}$$

$$A_1 = D_e T_s \frac{\phi T_s V_{HV}}{2L_{leak}}$$

$$A_2 = 0 \text{ for } V_{Cint} = \frac{1}{2} V_{HV} \frac{N_2}{N_1}$$

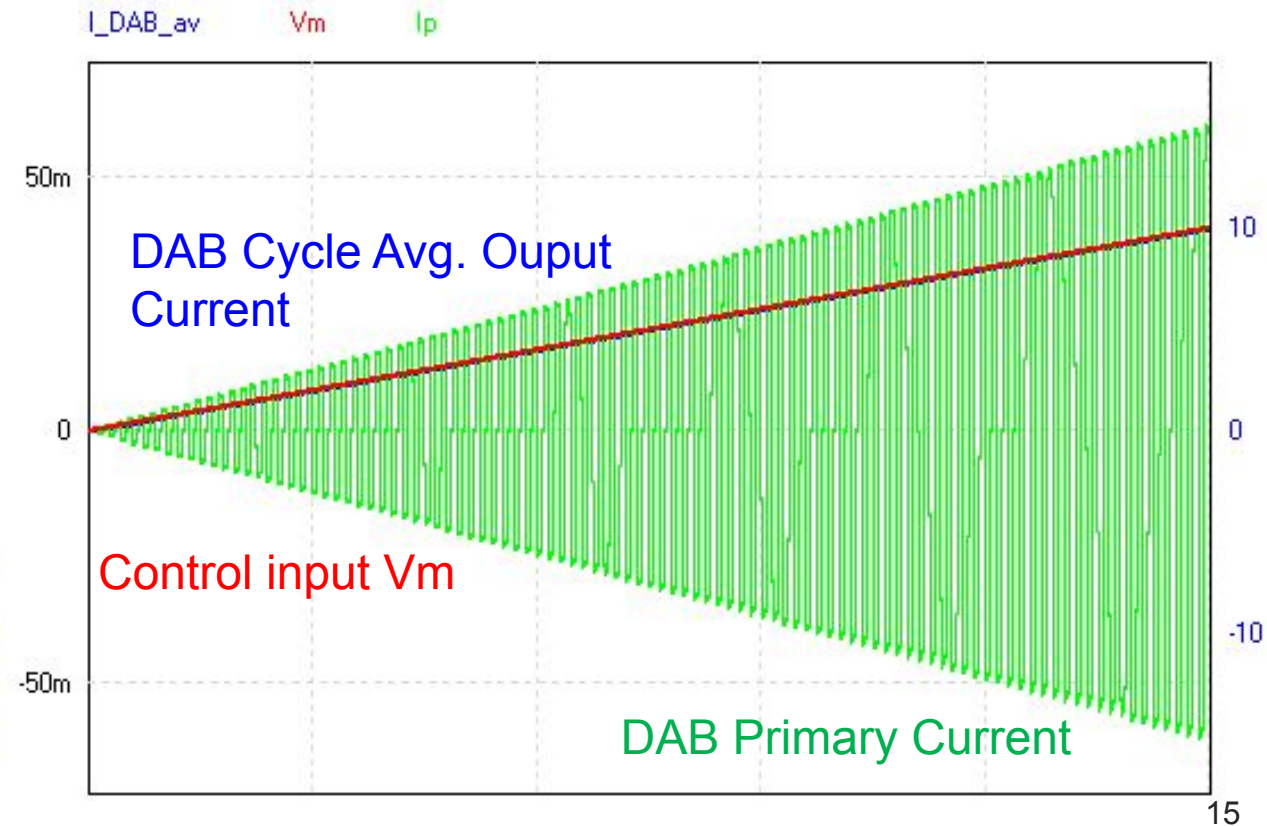
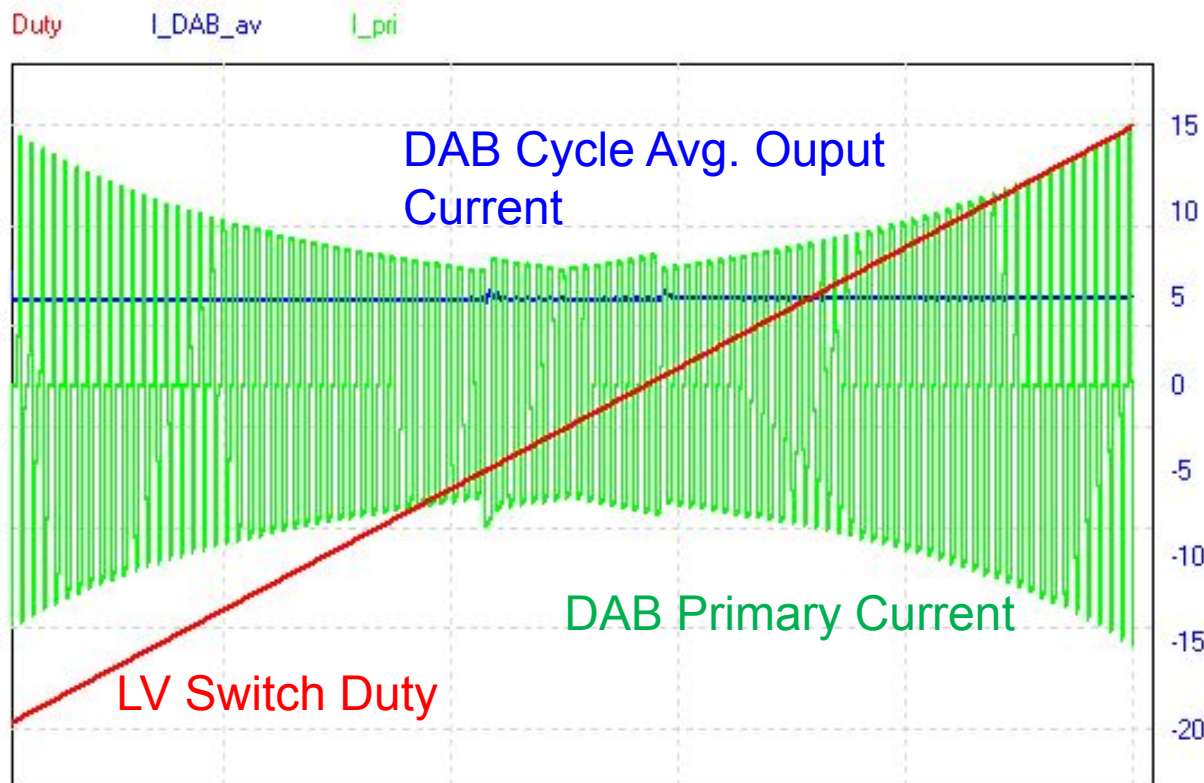


$$P_{DAB} \propto f(D_e) * \phi$$

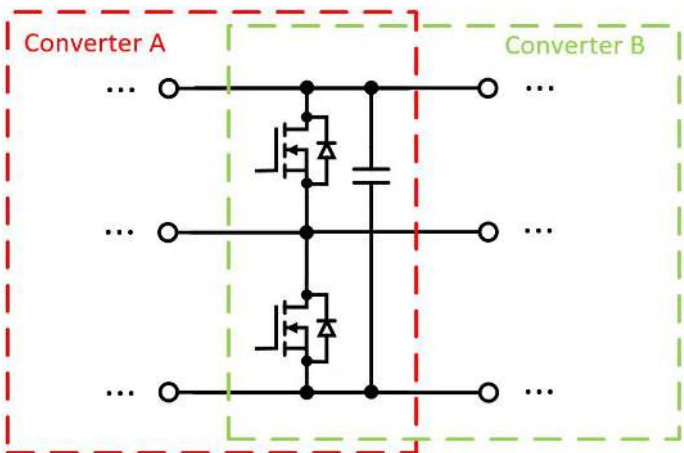
Define: $\phi = f^{-1}(D_e) * Vm$

Result: $P_{DAB} \propto Vm$ ★

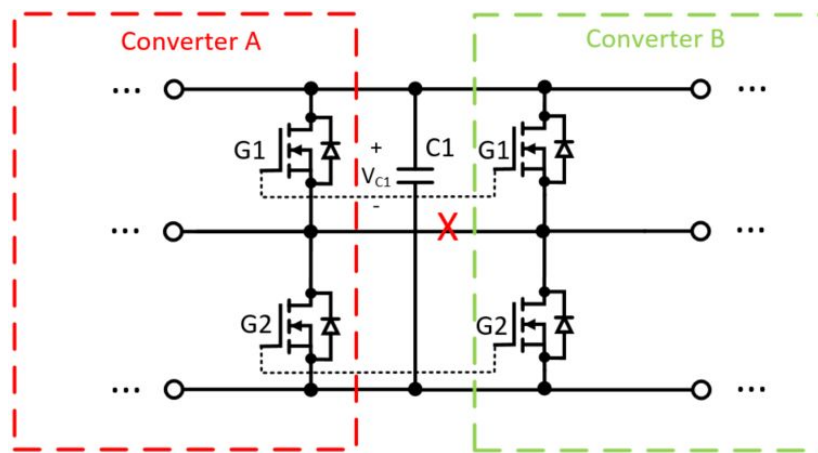
- DAB output current is fully decoupled from LV Duty
- DAB output current is directly proportional to control input V_m



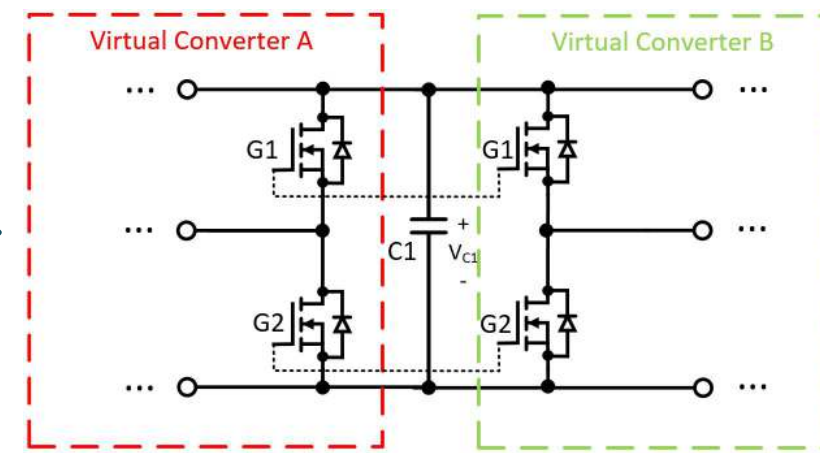
- Integrated converter analysis can be difficult due to interaction between stages at the shared components
- Virtual Converter Modeling (VCM) splits an integrated converter in to separate “virtual converters” which can be analyzed by traditional methods



Integrated Converter

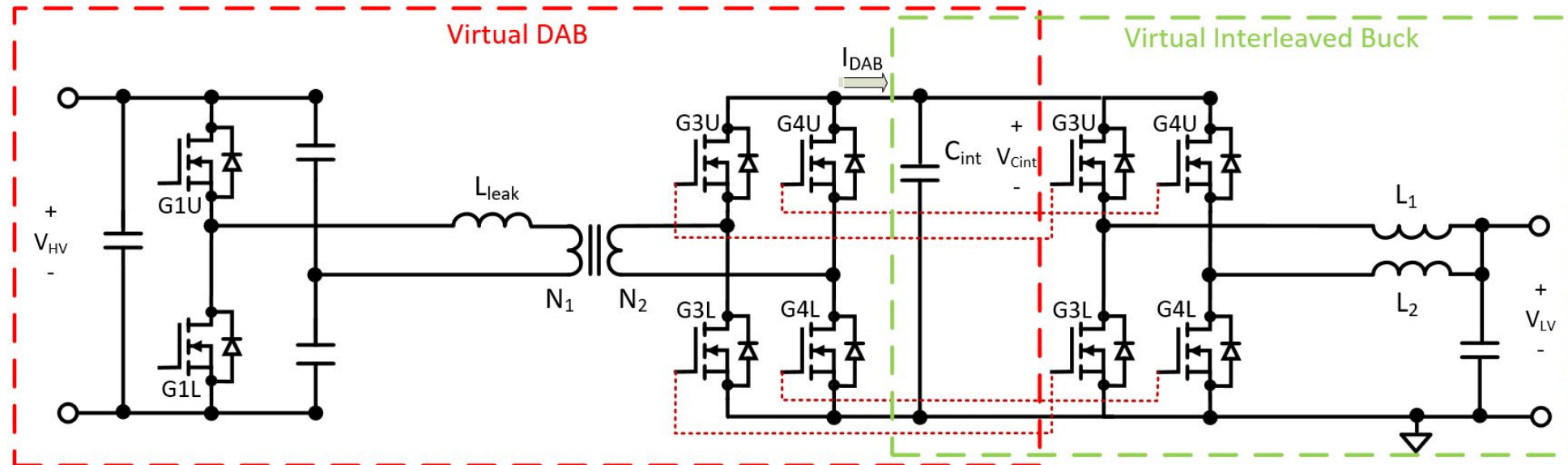


Switches duplicated,
gates connected



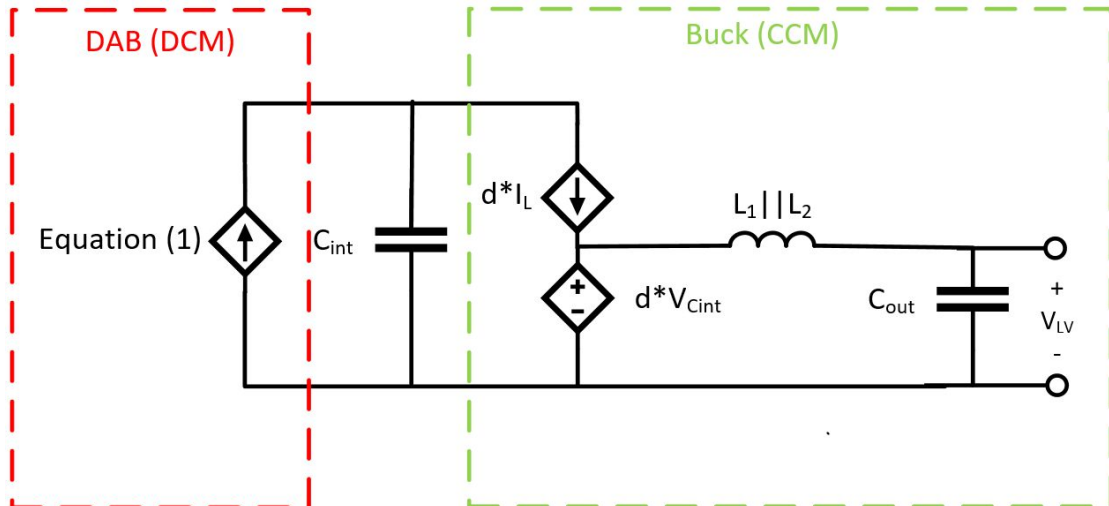
Virtual Converter
equivalent circuit

- Bidirectional Shared-Switch DC-DC Converter is modelled as separate DAB and Interleaved Buck
 - Additional constraint: LV bridge gates are driven in unison



- Large signal model is combination of standard DAB and buck models
 - DAB model derived by integrating transformer current (1)
 - Different operating modes (DCM vs. CCM) not an issue

$$I_{DAB} = \frac{2 * (A_1 + A_2) N_1}{T_s} \frac{N_1}{N_2} \quad (1)$$



$$\begin{bmatrix} \dot{V}_{Cint} \\ \dot{i}_{out} \end{bmatrix} = \begin{bmatrix} \frac{I_{DAB}}{C_{int}} & -\frac{di_{out}}{C_{int}} \\ \frac{2dV_{Cint}}{L_{buck}} & -\frac{2V_{LV}}{L_{buck}} \end{bmatrix}$$

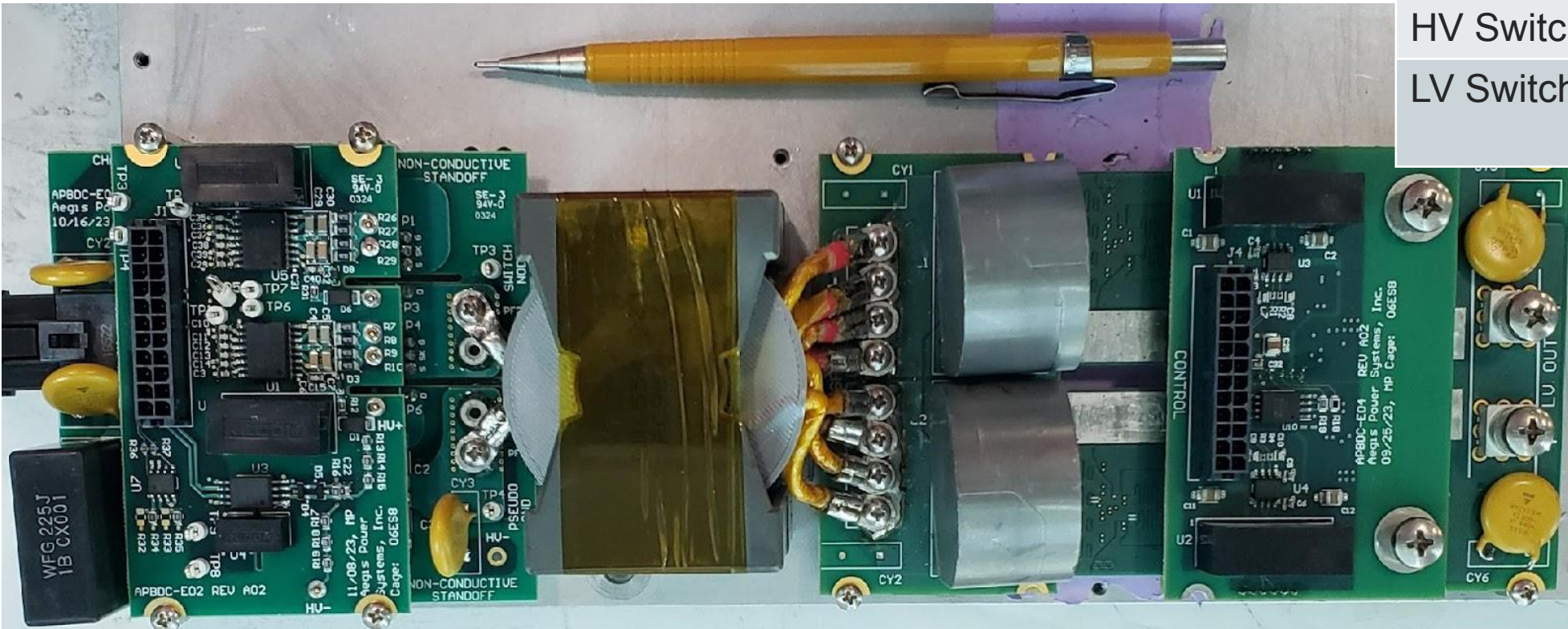
Large signal model and corresponding state space equations

- Small signal model can be derived from large signal state space equations

$$\begin{bmatrix} \tilde{V}_{Cint} \\ \tilde{i}_{out} \end{bmatrix} = \begin{bmatrix} \frac{\partial}{\partial V_{Cint}} \frac{I_{DAB}}{C_{int}} & -\frac{d}{C_{int}} \\ \frac{2d}{L_{buck}} & 0 \end{bmatrix} \begin{bmatrix} \tilde{V}_{Cint} \\ \tilde{i}_{out} \end{bmatrix} + \begin{bmatrix} \frac{\partial}{\partial \phi} \frac{I_{DAB}}{C_{int}} & \frac{\partial}{\partial d} \frac{I_{DAB}}{C_{int}} - \frac{i_{out}}{C_{int}} \\ 0 & \frac{2V_{LV}}{L_{buck}} \end{bmatrix} \begin{bmatrix} \tilde{\phi} \\ \tilde{d} \end{bmatrix}$$

- 600V to 28V DC-DC for military vehicles
- 4x parallel converters per module, 15kW total

Parameter	Value
Rated Power	3750 W
V_{HV}	565 – 635 V
V_{LV}	20 – 32 V
Switching Freq.	200 kHz
$N_1:N_2$	11:2
HV Switches	SiC, 1200 V, 31 A
LV Switches	GaN, 100 V, 101 A (2p top, 4p bottom)



- Shared-Switch converter topologies offer the benefits of a multi-stage converter with a reduced switch count
 - Lowered size, cost, and losses vs. independent stages
- A series connected DAB and Buck converter is well suited for heavy-duty electric vehicle applications
 - DAB provides isolation and bidirectional power control
 - Buck ensures DAB operates at maximum efficiency for all conditions
 - Proposed shared-switch configuration reduces switch count by 40%
- An innovative modulation method ensures linear power control and decoupling between stages
- Virtual Converter Modeling alleviates the difficulty of analyzing a shared-switch converter as a single circuit by superimposing simpler converter models

Thank you!